



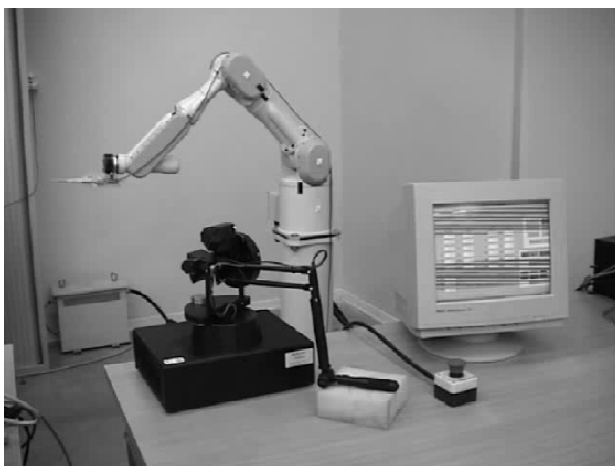
A Few Guidelines for the Design of Surgical Robot Arms

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Surgical Robot Arms: Master & Slave

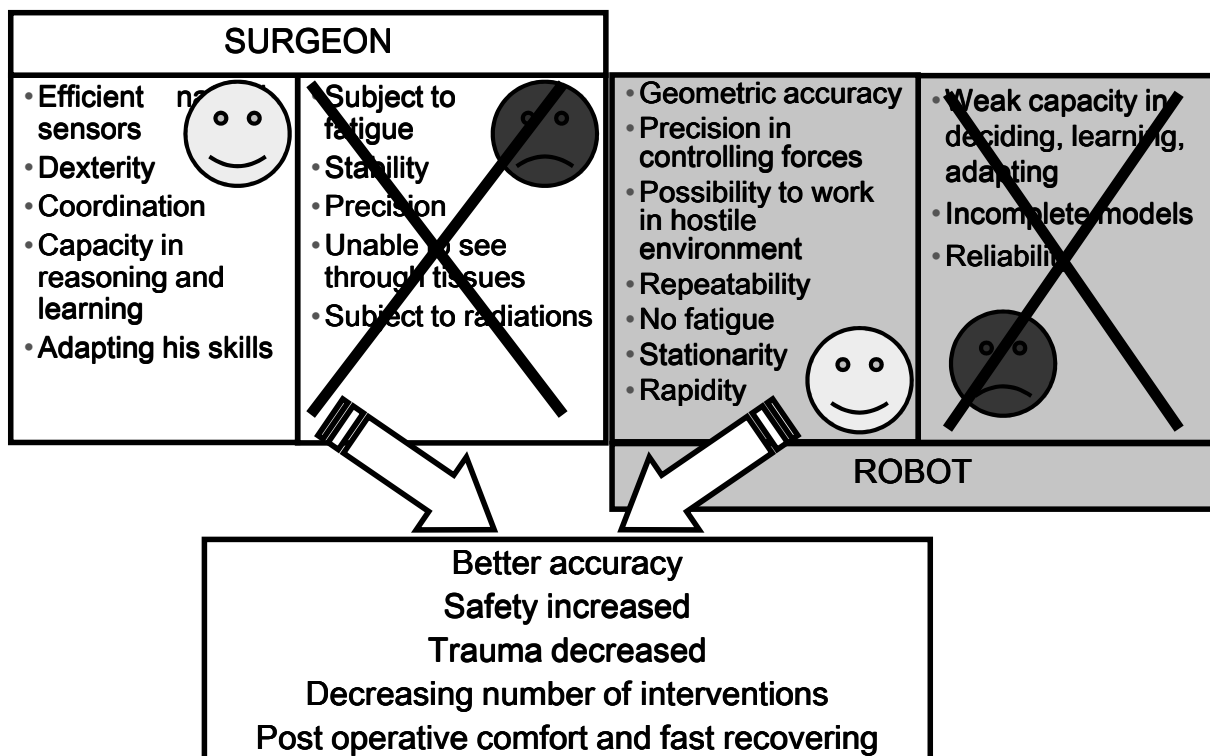




- A safety point of view
- Robot Arms
 - Classical Serial Arms
 - Not-so-classic Serial Arms
 - Parallel Arms
- Multi-purpose system?



A Safety Point of View





In contact with human body

- **Specific functionalities**
- **Easily movable**
- **Optimal size**
- **Manually controllable**

- **Unstructured environment,**
- **No repetitive tasks,**
- **Sterilization of the components...**



**Specific
safeties**

**Specific
kinematics**

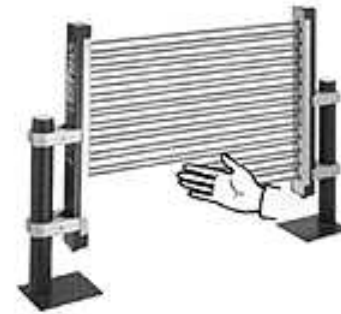


Industrial Robots

- Isolated from the workers (appropriate training to interact with them) by preventing machine workspace from human intrusion
- Possibility to enter in the workspace (for maintenance purpose or learning procedures) without stopping the machine:
 - Disconnecting of the protection devices
 - Activating the “manual mode” with limited speed

Medical Robots

- Medical robots cooperate with the human (surgeon and staff) and interact the patient
- Harsh constraints and specifications in the design itself, especially for active medical devices
- Influence of human factor and clinical constraints specific to mechanical devices for medical purpose



- Work done on human being:
 - Change in working conditions with each patient (characteristics of soft tissues, position of the patient on the operating table, size of the body and accessibility of the organs,...)
 - Task and execution specific to a patient: no “trial/error” nor “doing again” movements
- Robot directly in contact with the patient and staff:
 - Necessity of preoperative studies to plan the intervention
 - Modification of planning during the operation itself, according to the surgeon diagnostic, possible complications or patient organism behavior
- Surgeon is not “robotic specialists”:
 - Dedicated user-friendly HMI: task-oriented, allowing an easy manipulation of the system
 - Robot transparency: avoiding singularities, mechanical joint limits, reconfiguration procedures,...



- Every component of the system in contact with the sterile field must be sterilized (generally, the robot is covered by a sterile sleeve while the tool is separately sterilized by an autoclave procedure);
 - Environment is usually unstructured: operating rooms are cluttered with several other medical systems (radiology, anesthesia, surgery, etc.). The robot position with respect to the patient varies between two operations and even a single operation. Thus, its dimensions have to be reduced;
 - The robot has to be easily and quickly transportable in and out of the operating room
- Required functionalities are defined according to each kind of clinical operations → new medical robots have often been designed for specific operations;



- Any failure ⇒ very critical.
- Medical robots must function safely and with high reliability.
- 6 attributes of the concept of dependability :
 - Safety
 - Reliability
 - Availability,
 - Confidentiality,
 - Integrity,
 - Maintainability.

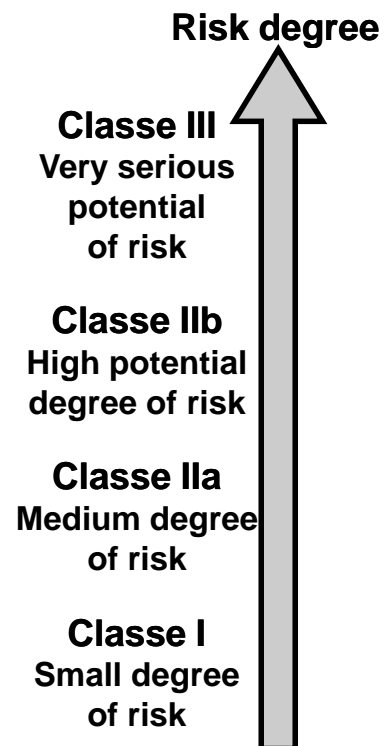


Safety rules: European Directives

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Guidelines for Design (11)

- In European Community: ISO 9000 norm has been modified to comply with the specific constraints of medical devices in the European directive 93/42/CEE.
- CE marking: the EN 46000 certification enacts the various criteria necessary to classify all the medical devices according to four classes.
- Device classification depends on:
 1. its life span use: from a few minutes (temporary) to several years (implantable)
 2. its invasiveness or non-invasiveness
 3. its surgical or non-surgical use
 4. its activeness or inactiveness
 5. the vital or non-vital body parts concerned by the device



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Emerging of a strategy ?

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Guidelines for Design (12)

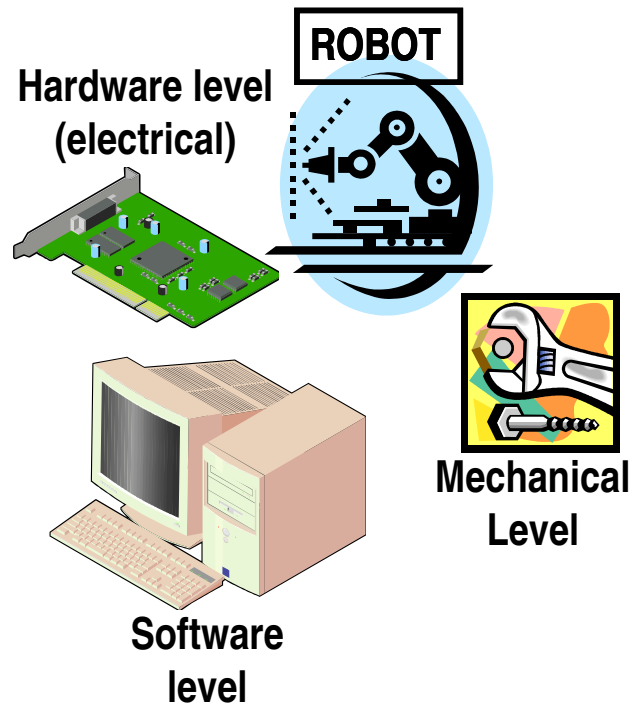
- In these directives, the “medical device” denomination includes several kinds of products such as drugs, compresses, electrical apparatus, mechanical devices, surgical or radiological tools,...
- Elementary rules for designing a “safe” surgical robot:
 - No uncontrolled motions
 - No excessive force on patient
 - Keep the surgical tool in a predefine workspace
 - Supervision by the surgeon of any motion
- To guarantee a high level of safety, a medical device such as a robot may be designed considering the main following principles:
 - The degree of redundancy in control and sensing
 - The possibility to design an intrinsically safe system (i.e. capacity to decrease the maximum level of risk by construction)
 - The tradeoff between reliability and safety. (... and cost)

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Emerging of a strategy ?

- Safety concepts based on three rules:
 1. Redundancy in sensor and control,
 2. Intrinsically safe components
 3. Reliability in design.
- Along three axis:
 1. At the electromechanical level
 2. At the hardware level
 3. At the software level



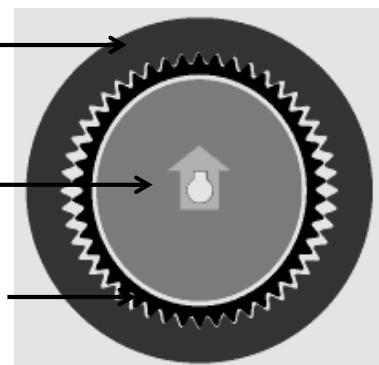
Electromechanical concepts of safety: Intrinsically safe components (1)

- Limitation of actuator power to satisfy only the required tasks better than simply using software thresholds to restrict payload, forces, torques, velocity and acceleration.
- Use of high reduction gears such as harmonic drives (high efficiency and low backlash) reduces the robot's velocity. But high reduction ratios \Rightarrow non back-drivable structures :
 - Required (in neurosurgery for instance)
 - Unacceptable (in remote MIS applications).

Circular Spline (N teeth)

Wave elliptic generator with ball bearing

Flexible Spline (N-2 teeth)





Electromechanical concepts of safety: Intrinsically safe components (2)

- For systems applying effort: when the robot force becomes too important, a mechanical system (“mechanical fuse”) enables to quickly drop the tool. (On AESOP, the collar linking the endoscope and the arm is quickly disconnected thanks to a magnetic connection).
- Joints may also be equipped with mechanical torque limiters mounted on the motor shaft (e.g. Neurobot or Hippocrate): when a link collides with an obstacle during a motion, it stops moving while the motor shaft still rotates.



Electromechanical concepts of safety: Intrinsically safe components (3)

- In case of power breakdown or emergency stop, parking brakes mounted on selected joints prevent the robot from falling down under gravity effect.
- However, this technical choice presents a main drawback: when the user has to manually move the arm without actuator control, the brakes have to be released. Besides, many robots tend to vibrate a bit when brakes are applied.
- As an alternative to this solution, gravity compensation may be fulfilled by a passive counterbalancing payload or by a full irreversible structure



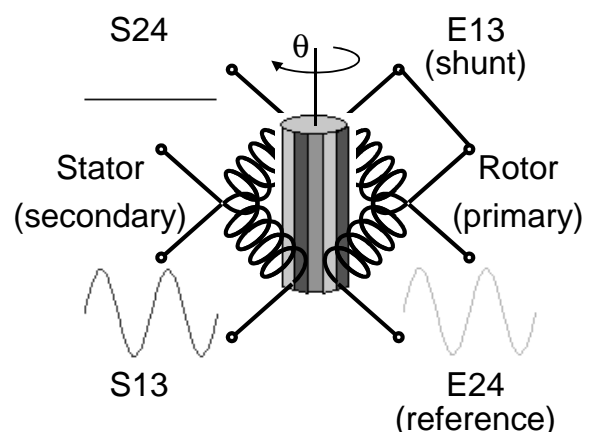
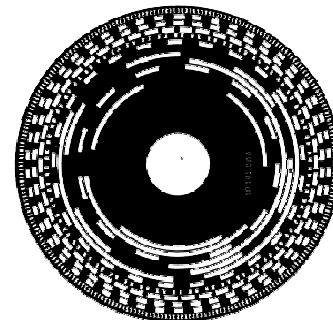
Electromechanical concepts of safety: Redundancy of sensors (1)

- Decreasing the hazard rating \Rightarrow Increasing information and improving control by using redundant and independent components.
- Examples:
 - Stereotactic neurosurgery during the needle insertion phase \Rightarrow duplication of joint brakes to prevent any breakdown effect
 - In Image Guided Surgery applications \Rightarrow using both independent active and passive marker-based tools to improve the reliability of the tracking system (e.g. cameras coupled with a Computed Tomography system)



Electromechanical concepts of safety: Redundancy of sensors (2)

- Avoided time consuming and potentially hazardous initialization procedures by using:
 - one absolute joint position sensor
 - a combination of two relative encoders (one sensor mounted on the motor output shaft and the other mounted on the joint axis)
- Examples:
 - two resolvers (Hippocrate, SCALPP,...)
 - one incremental encoder associated with an absolute encoder (Robodoc)
 - one incremental encoder associated with potentiometer (NeuroSkill robot, SCALPP,...).
- Redundancy of sensors also used for the arm control: e.g. information on the joint velocity deduced thanks to the coarse sensor.





- Avoid the risk of wrenching or cutting wires, by shielding and integrating all leads inside the links of the robot arm.
- Limiting the working envelope by using mechanical joint limits: physical threshold (+ software threshold).
- Computer Aided Design analysis for selecting robot location
- Kinematics concept:
 - Adapting the number of dof to the required task workspace
 - ... or use redundant kinematics to avoid collision and increase dexterity (for instance, in MIS or in neurosurgery)
 - Fit link dimensions to preserve patient and clinical staff safety
 - Kinematic models:
 - Avoid numerical or polynomial resolution methods and prefer analytical ones
 - Reject wrist and shoulder singularity configurations out of the workspace as much as possible



- Safety at “electrical level”
 - Intrinsically safe components
 - Redundancy
 - Wiring techniques
 - EMC ... and so on
- Safety at software level
- Safety at system monitoring level

(see IEEE Magazine for more on that ...)

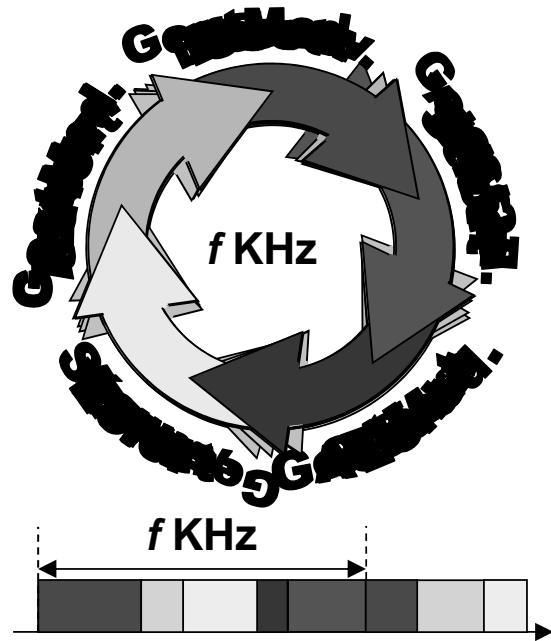


Software concepts of safety: Real-time controller

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Guidelines for Design (21)

- Design the controller as concurrent processes dedicated to specific tasks: security, Cartesian control, joint control, communication with peripheral units and sensors, HMI communication,...
- By tuning the process and variable priorities, an appropriate emergency procedure is switched on as soon as an error is detected. For instance, the dedicated security process may have the higher priority.
- → Stable computation time → closed-form solutions for models.



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Safety ... then what ?

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Guidelines for Design (22)

With safety in mind, you still have to
select which arm to use...

A classic (means: serial)?

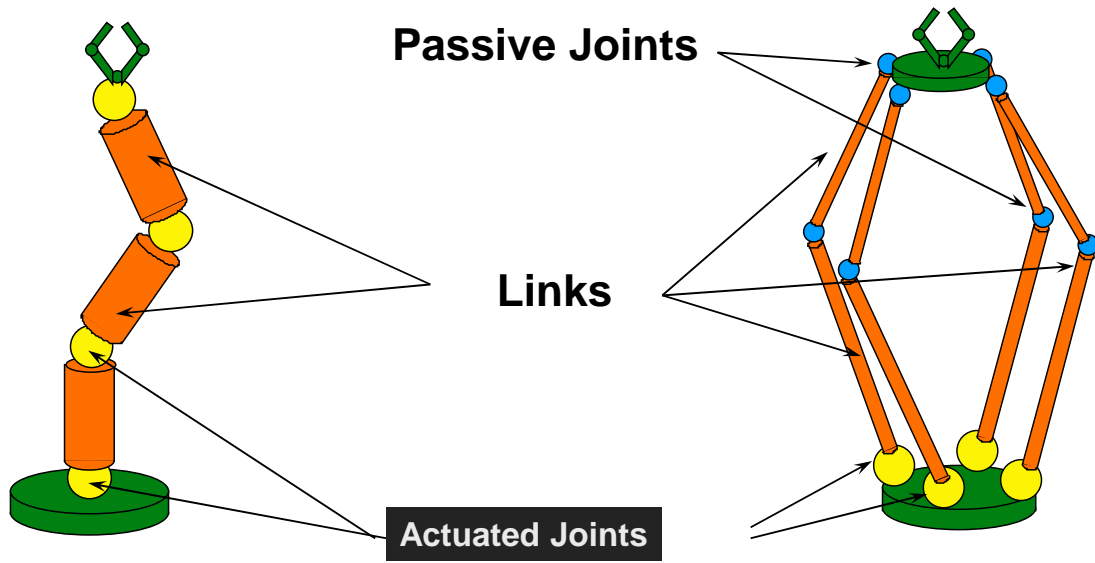
A not-so-classic?

A PKM?

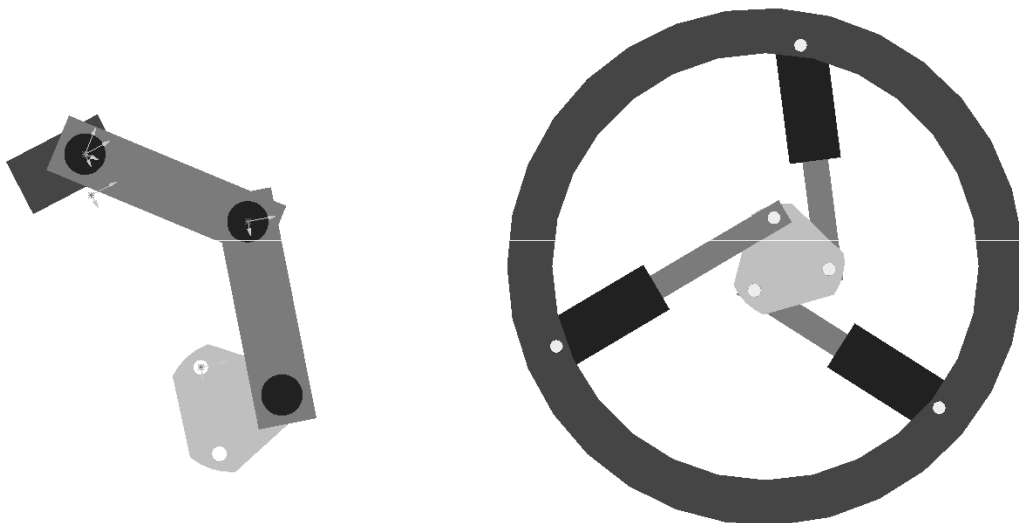
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PKM versus Serial



PKM & Serial in Motion

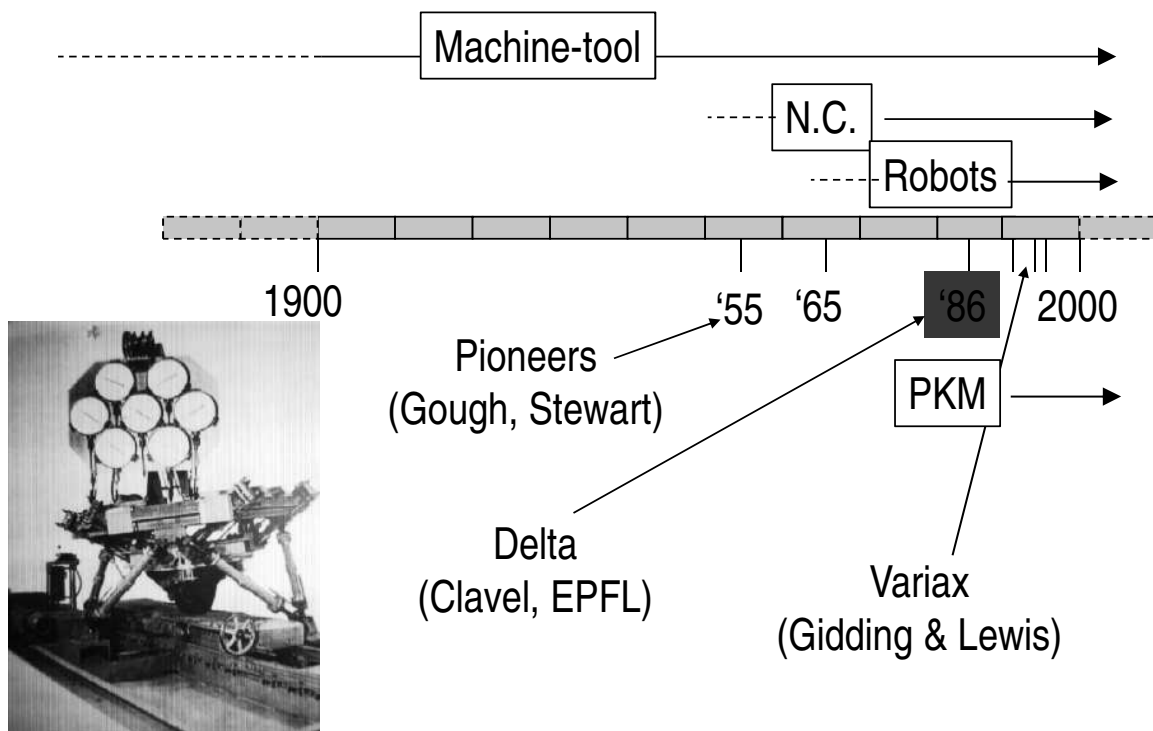




Historical Perspective

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Guidelines for Design (25)



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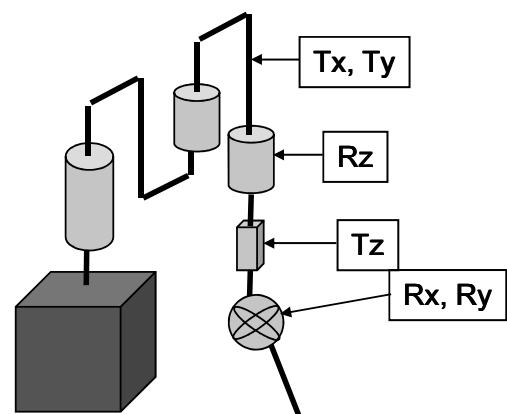
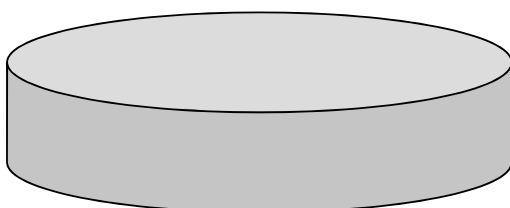


Classical Serial Arms

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Guidelines for Design (26)

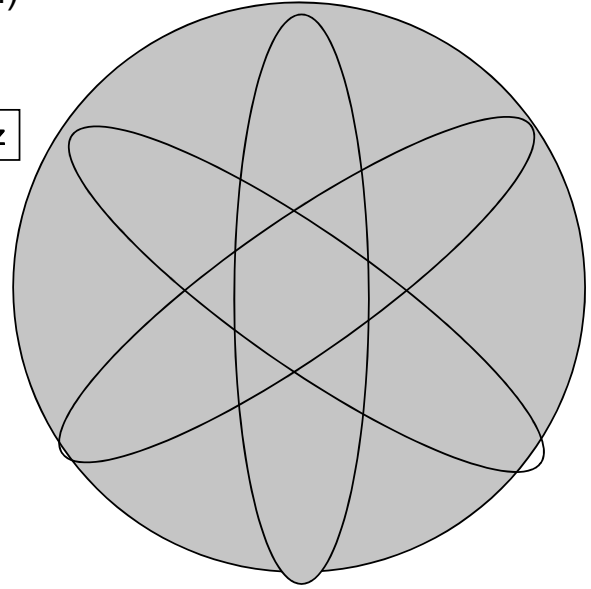
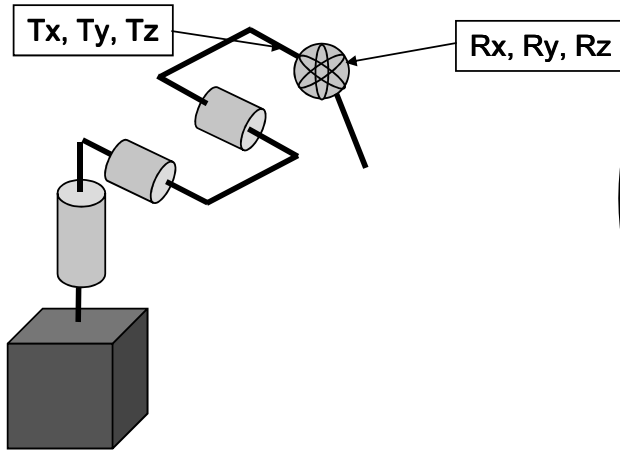
- Two important “families”:
 - Scara
 - Anthropomorphic
- Scara:
 - Comes from “pick-and-place” applications
 - 4 dof + possible 1~2 dof “wrist”
 - Workspace \Leftrightarrow “flat” cylinder



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- Anthropomorphic Arm
 - Comes from automotive industry applications (painting, welding)
 - A carrier (3dof) + a “wrist” (2~3dof)
 - Workspace \Leftrightarrow a sphere



Scara



Anthropomorphic

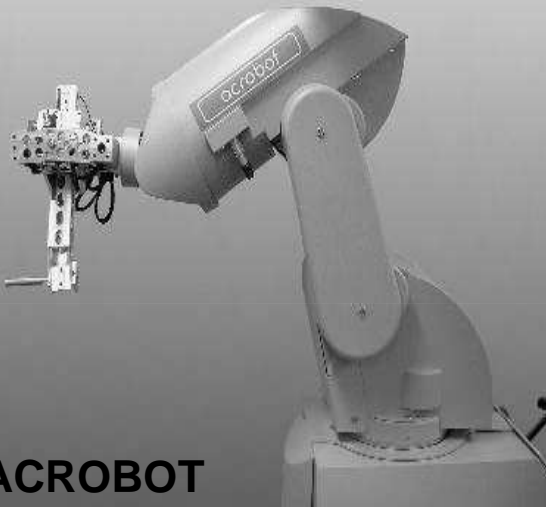




Scara & Anthropomorphic in Surgery

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Guidelines for Design (29)



ACROBOT

Anthropomorphic
Or
Anthropomorphic-like



Neuromate

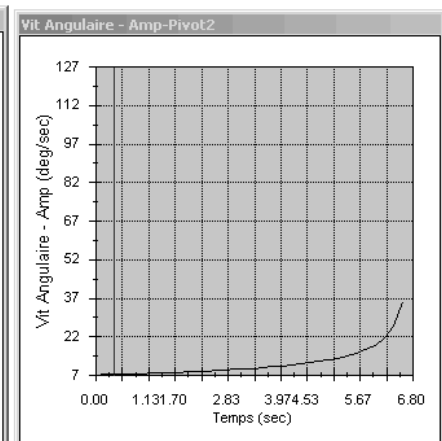
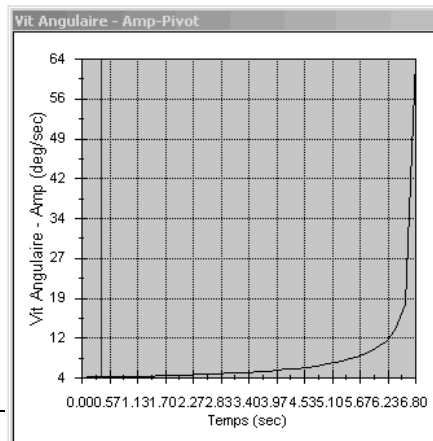
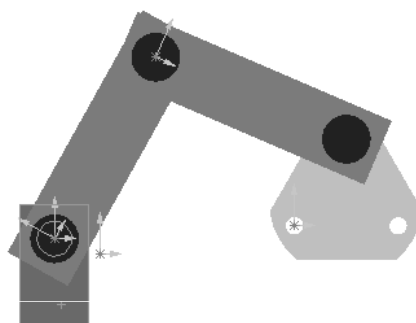


Classical Arms Key Features

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Guidelines for Design (30)

- Scara & A-R ⇔ the “foundation” of robotics (100% mastered)
- Transformation models are OK
 - F.K. is straightforward
 - I.K. just a bit more tricky
- Singular positions exist



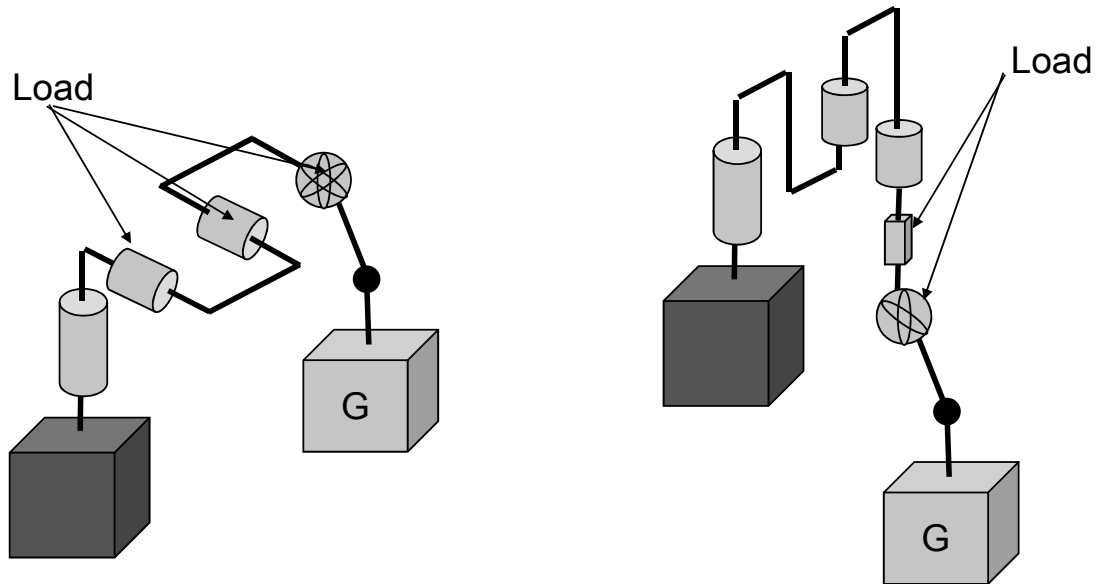


Scara vs Anthropomorphic

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Guidelines for Design (31)

- Scara presents less problem with Gravity effects



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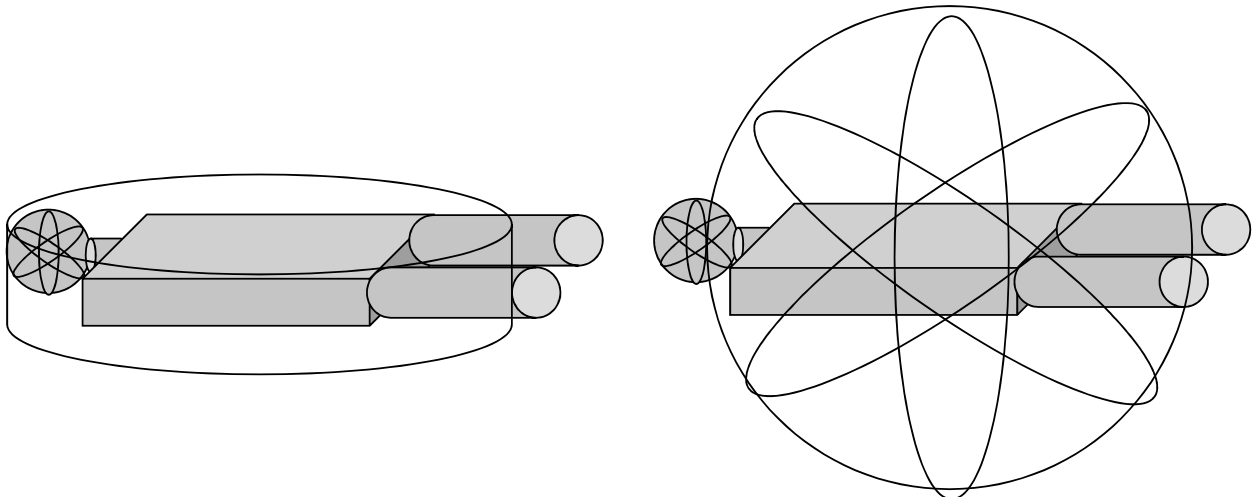


Scara vs Anthropomorphic

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Guidelines for Design (32)

- Scara's workspace is more likely to suit to the volume of a human body lying on a surgical table

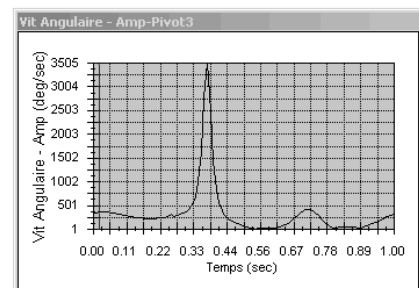
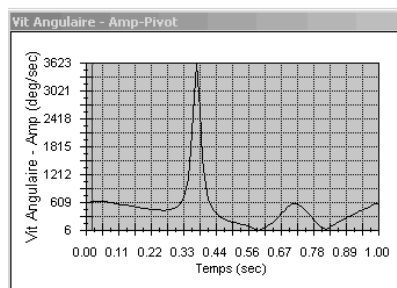
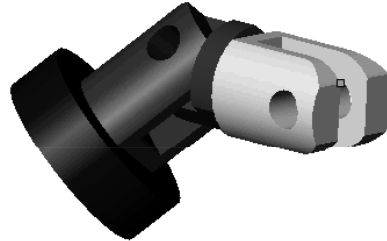


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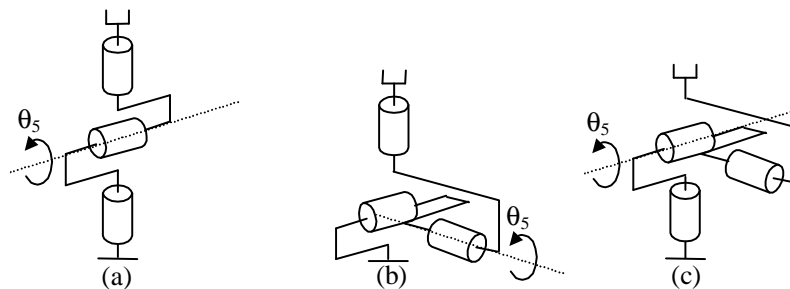


Scara vs Anthropomorphic

- It is possible to design an almost-singularity-free Scara arm
 - Most problems come from “wrist singularity”
 - Typical case: axis 4 and 6 aligned
 - One way out of this problem: non spherical wrists
 - New problem: I.K. in closed form?



One offset is not enough



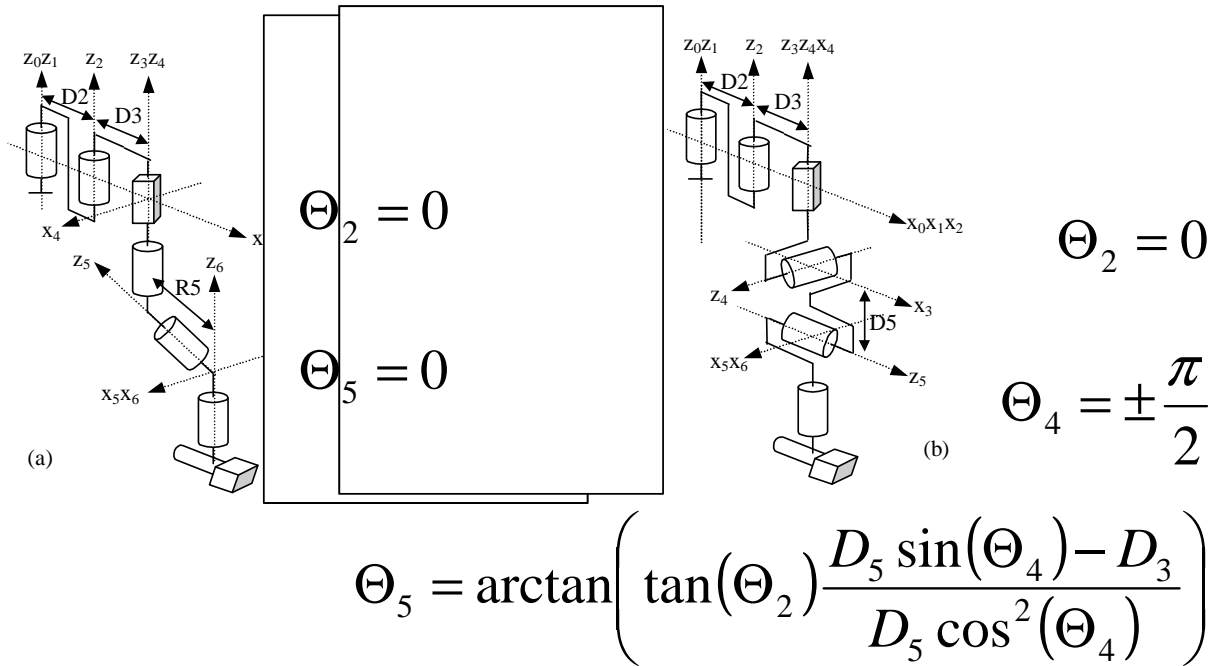
$$\Theta_5 = 0$$

$$\Theta_5 = \pm \frac{\pi}{2}$$

- Symmetric joint limits?
- Ranges of motion?

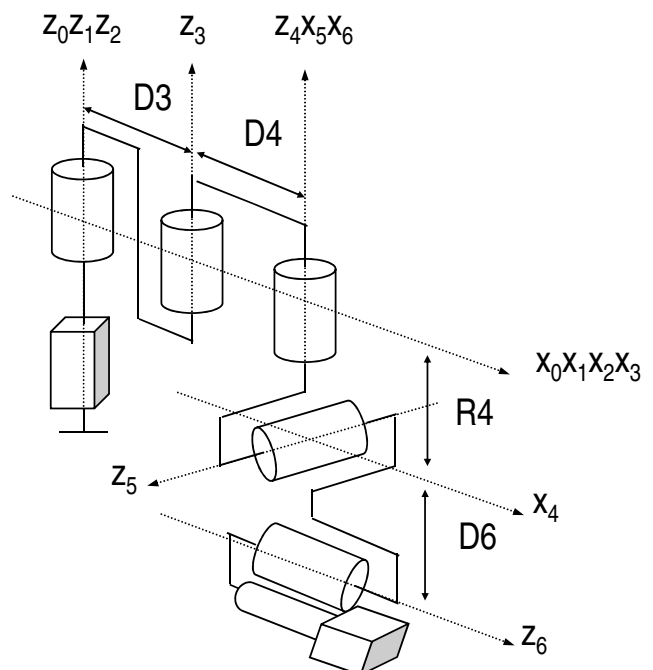


Most non-spherical wrists aren't OK



... but one design does it all

- 6-degree-of-freedom Scara Robot,
- No wrist-singularity,
- One classical singularity on the elbow,
- Inverse Kinematics Model,
- Non-spherical wrist,
- Large Workspace.





Easy singularity check + I.K. in closed form

$$\star \det(\mathbf{J}) = D_3 D_4 \sin(\Theta_3) \cos(\Theta_5)$$

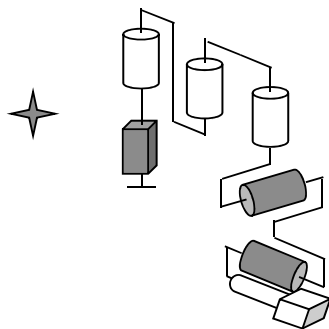
$$\star U_0 = \begin{bmatrix} s_x & n_x & a_x & p_x \\ s_y & n_y & a_y & p_y \\ s_z & n_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



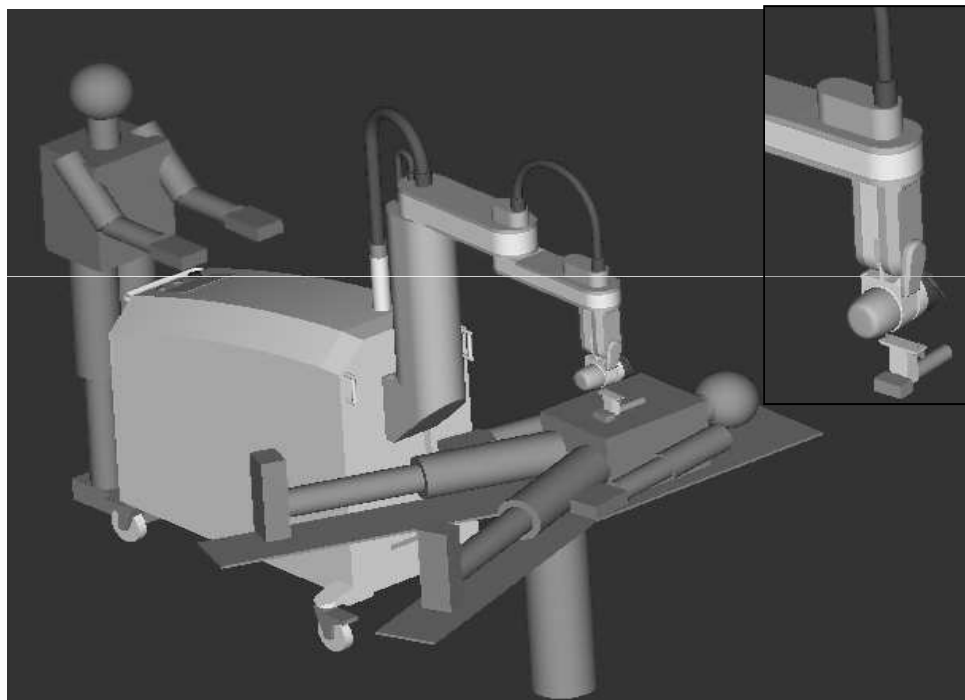
$$\theta_5 = \text{atan2}\left(a_z, \pm\sqrt{n_z^2 + s_z^2}\right)$$

$$\theta_6 = \text{atan2}\left(\frac{-n_z}{C_5}, \frac{s_z}{C_5}\right)$$

$$r_1 = p_z - R_4 - D_6 C_5$$



Scalpp Kinematics

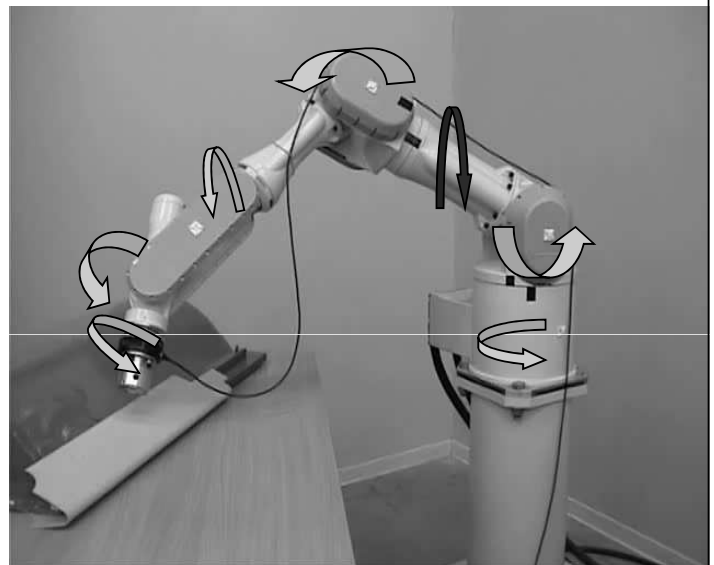
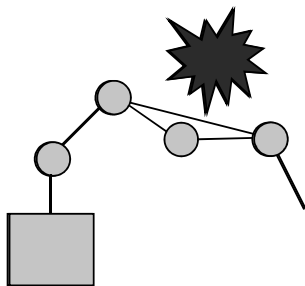




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- Redundant Arms
 - Offer more dof than strictly needed
 - May help to avoid collisions



- “Numerically tricky” (The I.K. is not solvable in closed form)

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Solving I.K. for Redundant Arm

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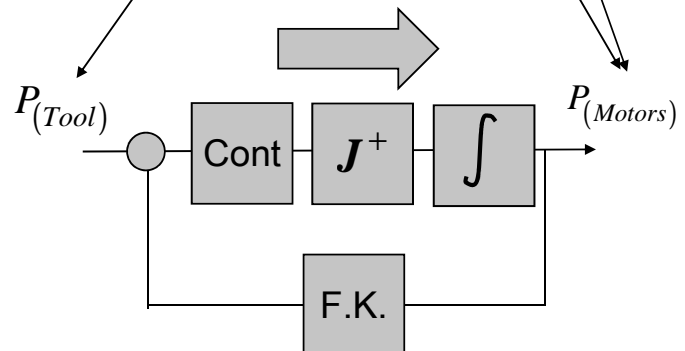
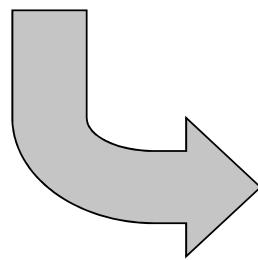
Guidelines for Design (41)

$$V_{(Tool)} = \mathbf{J} V_{(Motors)}$$

Not a SQUARE matrix!

$$V_{(Motors)} = \mathbf{J}^+ V_{(Tool)}$$

Pseudo-inverse



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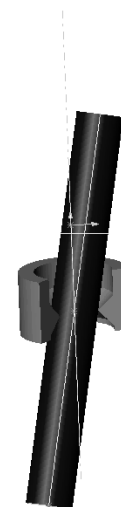


Not-so-classic Serial Arms

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Guidelines for Design (42)

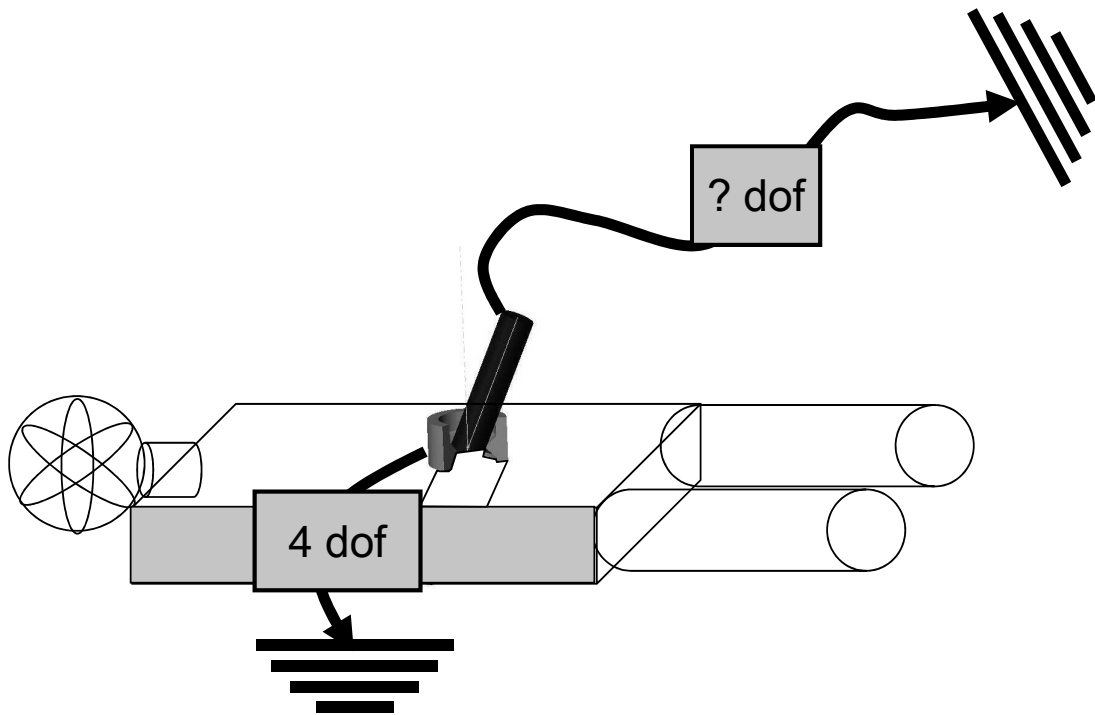
- Arms with kinematics constraint
 - The idea is to create a mechanical structure able to give the tool one SPECIFIC type of motion
 - Mostly applied to mini-invasive surgery
- M.I.S. → a tool (shape ⇔ cylinder) passes through a trocar (shape ⇔ annulus ??)
- The tool axis always passes in one “fixed” point
- → Two constraints (translation is constrained in two directions)



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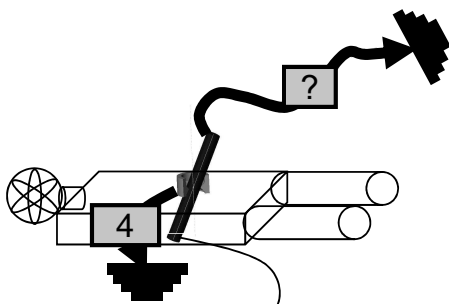


How many dof for respecting the constraints?



How many dof for respecting the constraints?

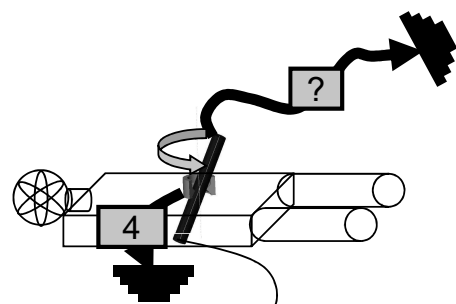
- Gruebler formula: $Mobility = (Total\ dof) - (6 \times Nb\ of\ loops)$



Mobility \rightarrow Tx, Ty, Tz \rightarrow 3

$$3 = (4 + ?) - (6 \times 1)$$

$$\rightarrow ? = 5$$



Mobility \rightarrow Tx, Ty, Tz, Rz \rightarrow 4

$$4 = (4 + ?) - (6 \times 1)$$

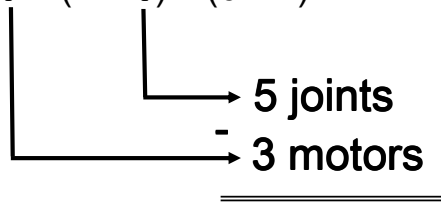
$$\rightarrow ? = 6$$



Option 1: passive joints

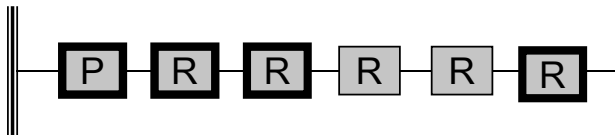
- Mobility \rightarrow Tx, Ty, Tz \rightarrow 3

- $3 = (4 + 5) - (6 \times 1)$



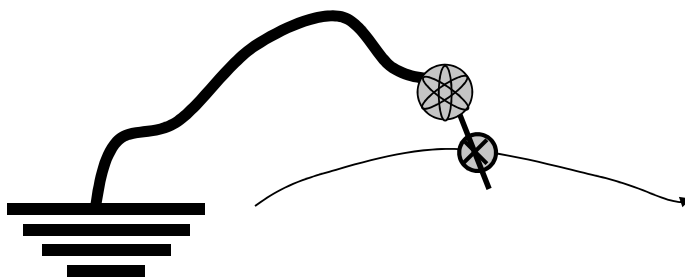
2 passive joints

Zeus



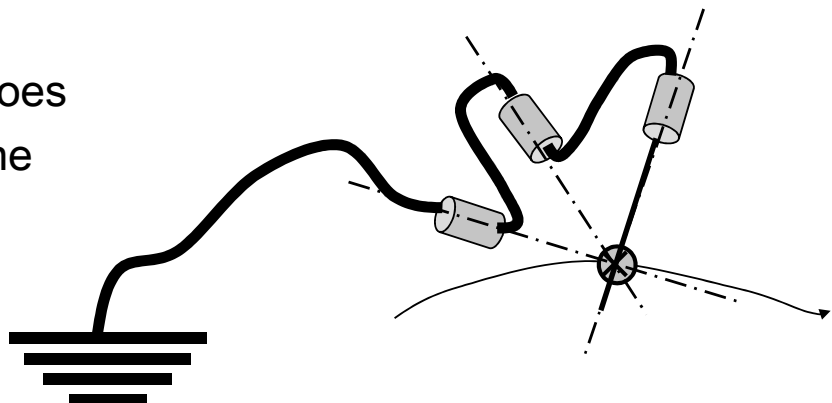
Option 2: Remote Rotation Center

- A classical spherical wrist does not rotate at the “right” point



- A RRC system does and thus “cancel” the Constraint

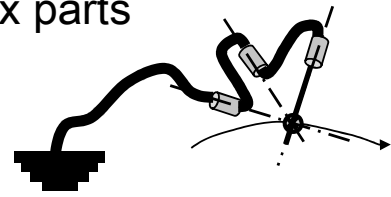
- $3 = (6 + 3) - (6 \times 1)$



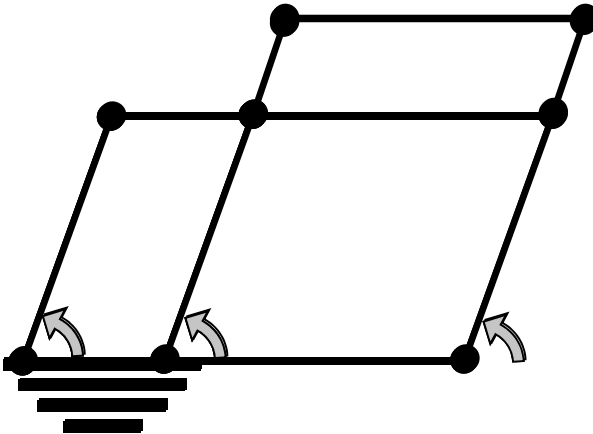


RRC or “The Magical Parallelogram”

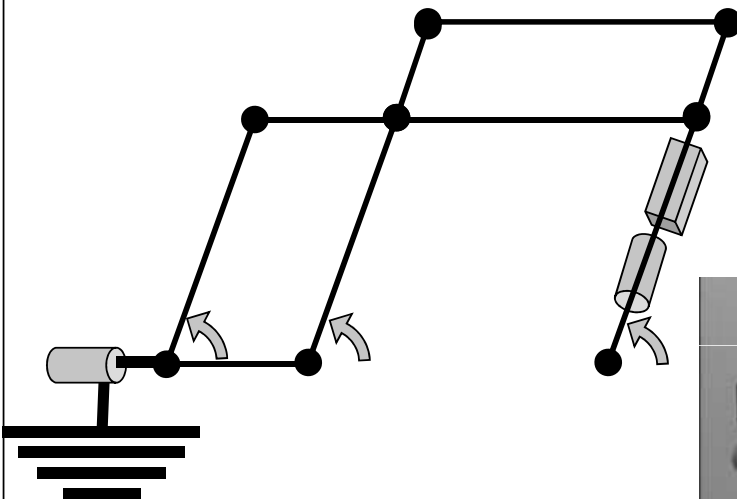
- RRC with spherical links requires complex parts



- ... while a basic parallelogram may do the job as well



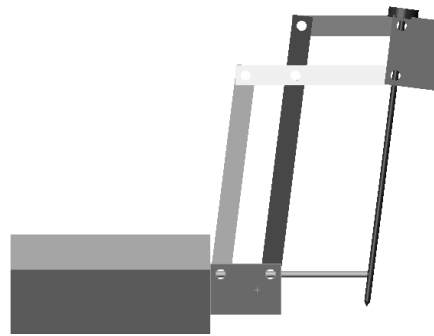
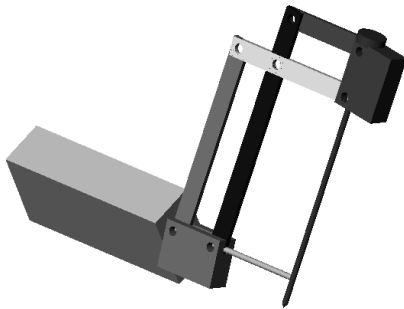
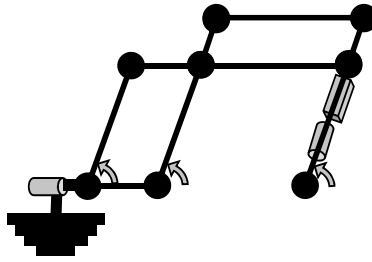
Implementation of RRC



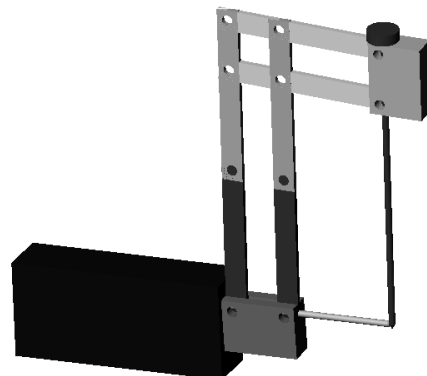
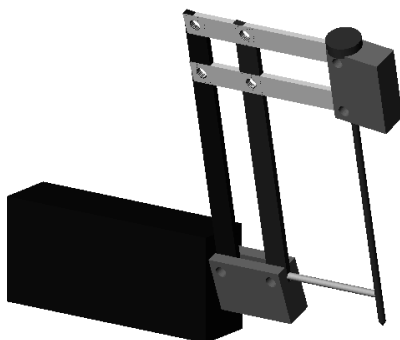
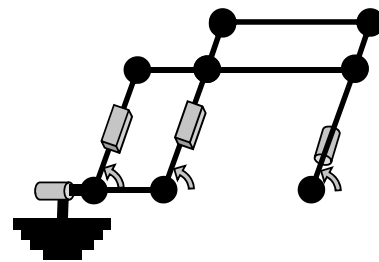
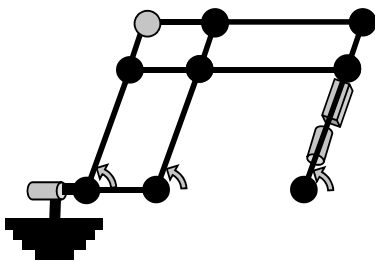
Da Vinci



RRC in motion

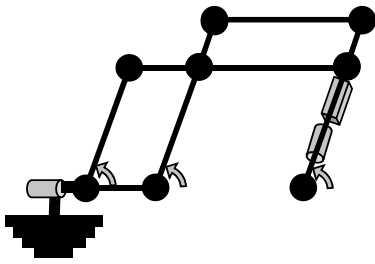


RRC: other "unique" solutions...

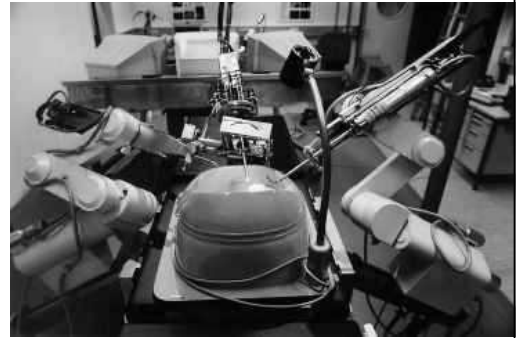
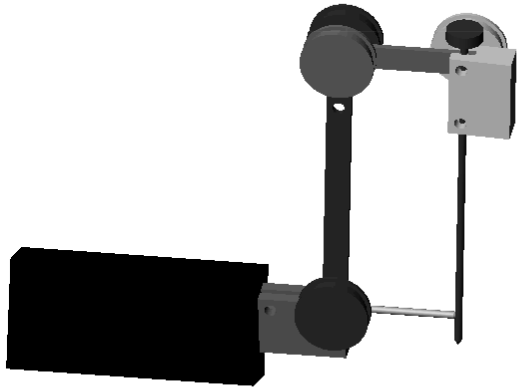
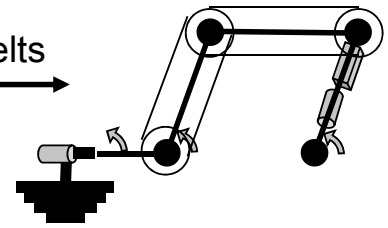




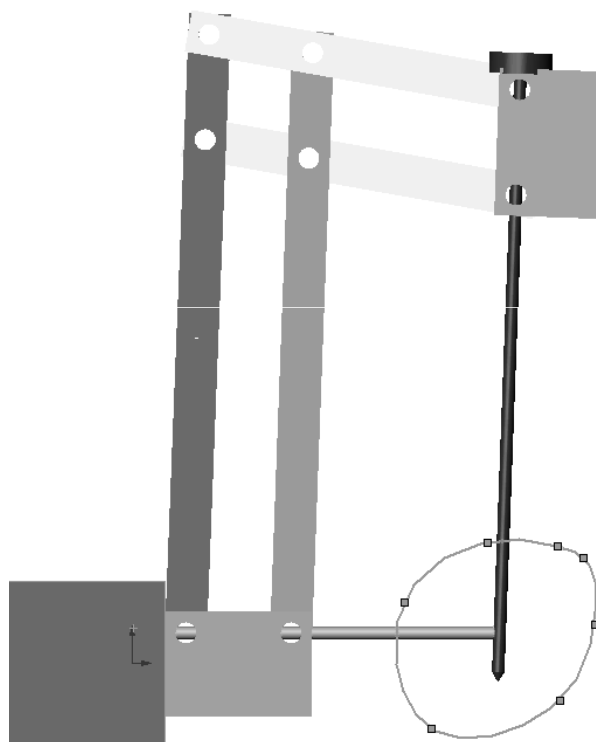
RRC: other "unique" solutions...



From solid links to timing belts



Remark: the parallelogram must be a real one!



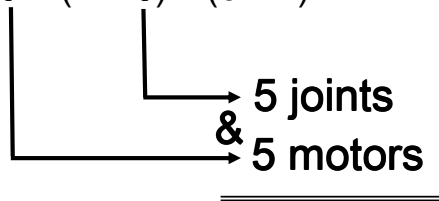


Option 3: force control

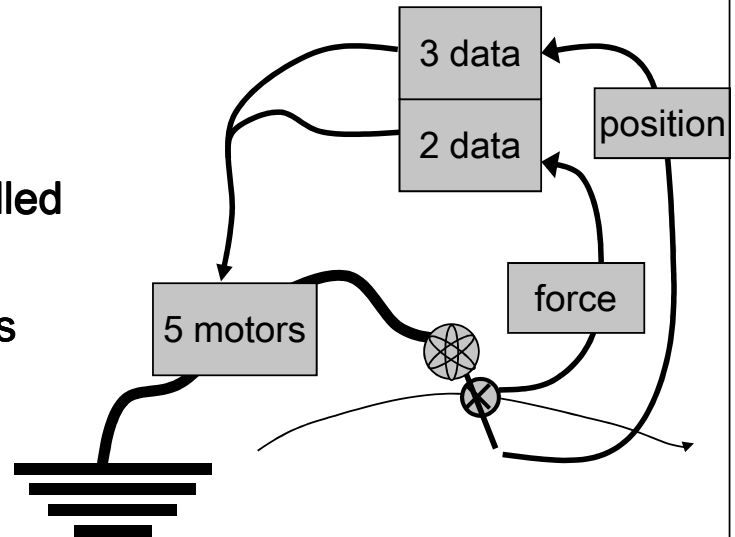
LIRMM

Guidelines for Design (53)

- Mobility \rightarrow Tx, Ty, Tz \rightarrow 3
- $3 = (4 + 5) - (6 \times 1)$



2 dof controlled
with force
measurements



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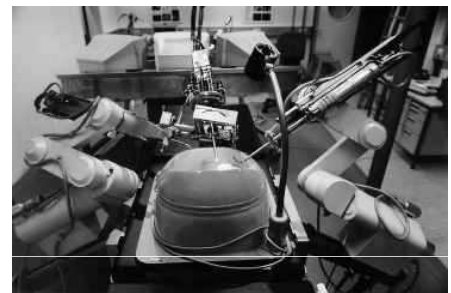


Overview of arms with kinematics constraint

LIRMM

Guidelines for Design (54)

- Option 1 (passive joints)
 - Few motors
 - The trocar “forces” the passive joint to adapt “mechanically”
 - No accurate positioning is needed
- Option 2 (RRC)
 - Few joints and motors
 - The trocar has no influence on the arm motion
 - BUT, the arm MUST be precisely located (positioning device + procedure)
- Option 3 (force control)
 - The trocar “forces” the passive joint to adapt by means of measures + control software
 - A bit more complex
 - May open a path to “multi-purpose” systems



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Overview of Serial Arms

LIRMM

Guidelines for Design (55)



ROBODOC



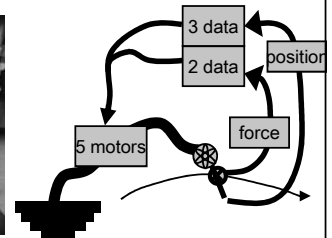
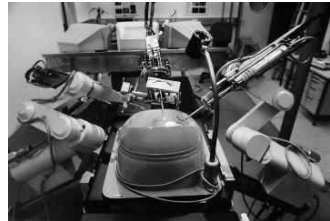
CASPA



Zeus



Da Vinci



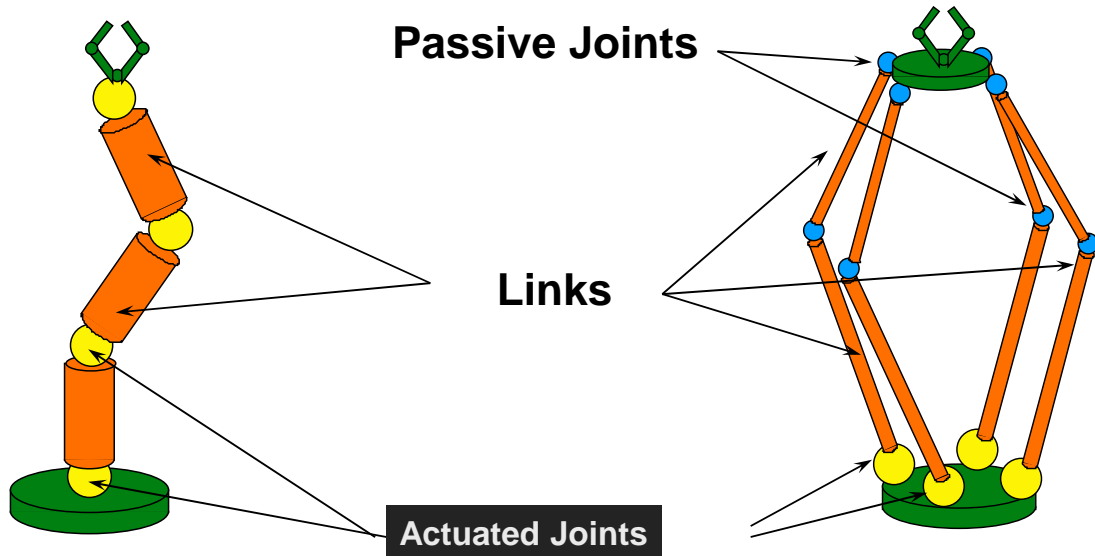
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... Still half the way to go ...

LIRMM

Guidelines for Design (56)



Passive Joints

Links

Actuated Joints

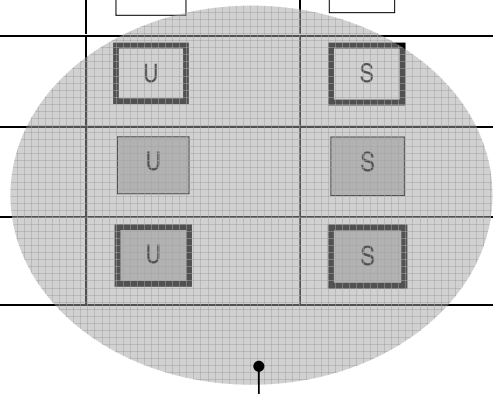
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- The PKM Landscape - A Convention to Describe PKM

	Revolute	Prismatic	Universal	Spherical
Passive	R	P	U	S
Passive + measurement	R	P	U	S
Actuated	R	P	U	S
Actuated + measurement	R	P	U	S

table 1. Symbols for Joint-and-Loop graphs.



(not easy to implement)

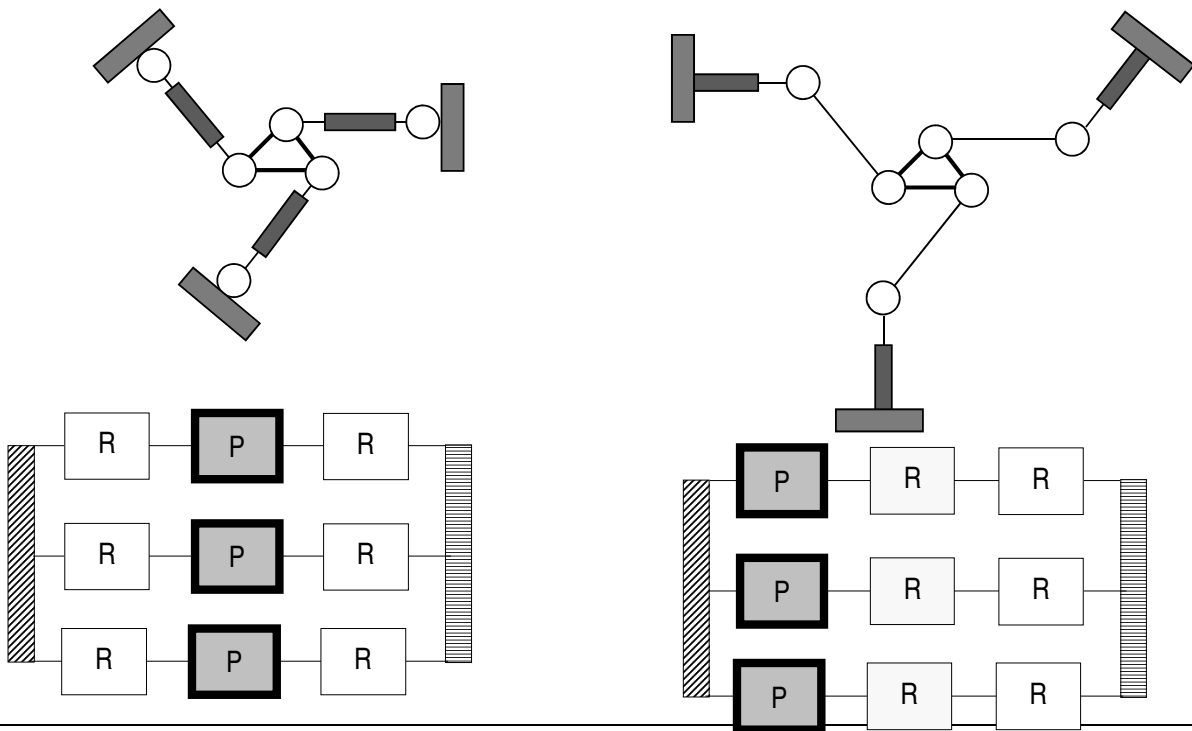


An example (H4)

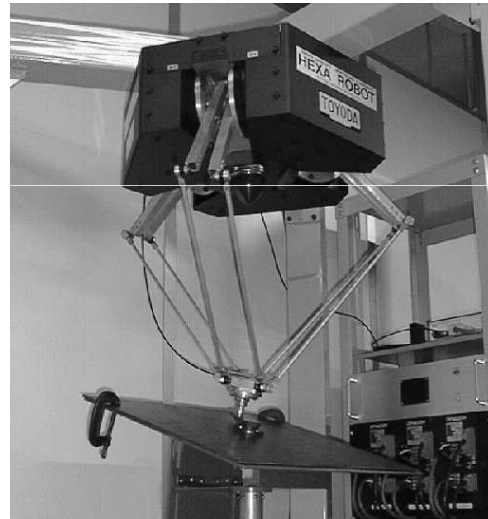
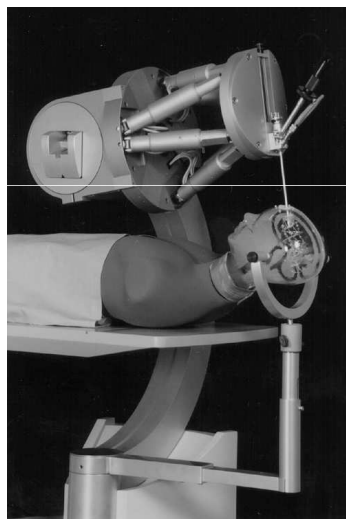




- The PKM Landscape - Telescopic Legs or Fixed-Length Legs



- The PKM Landscape - Telescopic Legs or Fixed-Length Legs

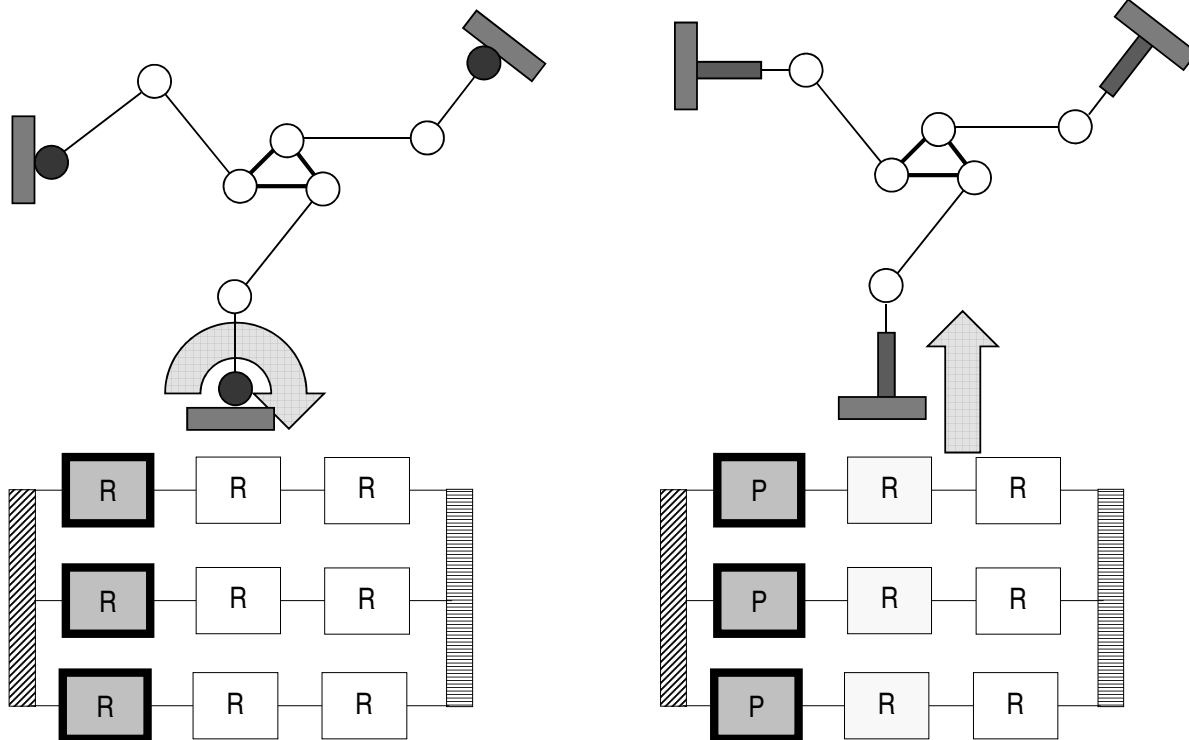




- The PKM Landscape - Rotational or Linear Drives

LIRMM

Guidelines for Design (61)



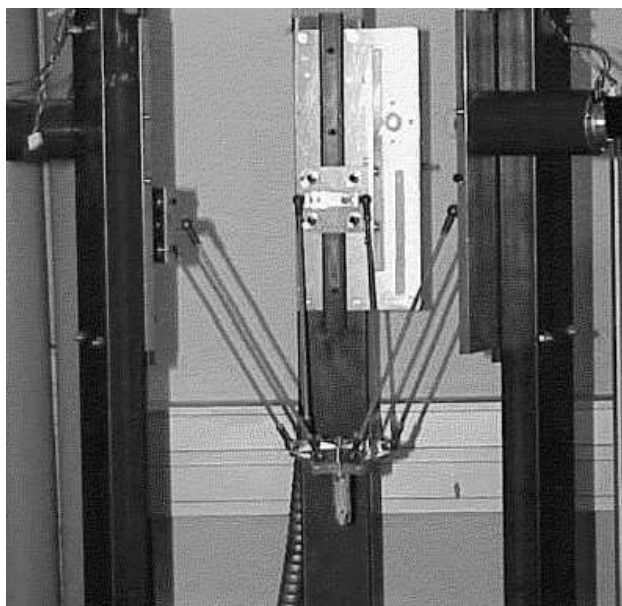
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- The PKM Landscape - Rotational or Linear Drives

LIRMM

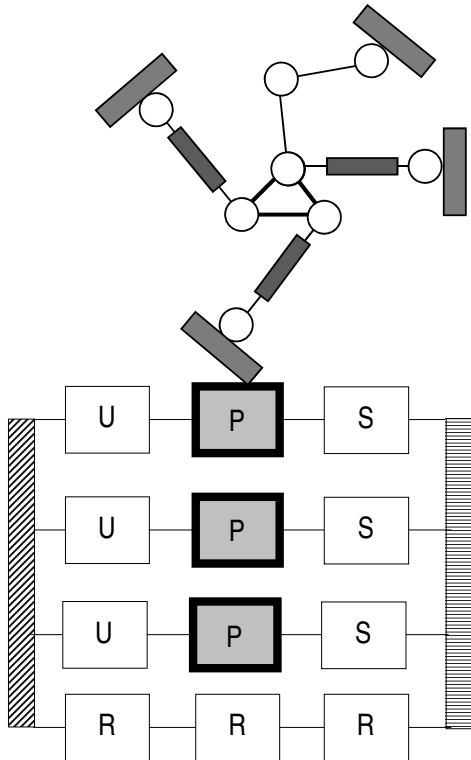
Guidelines for Design (62)



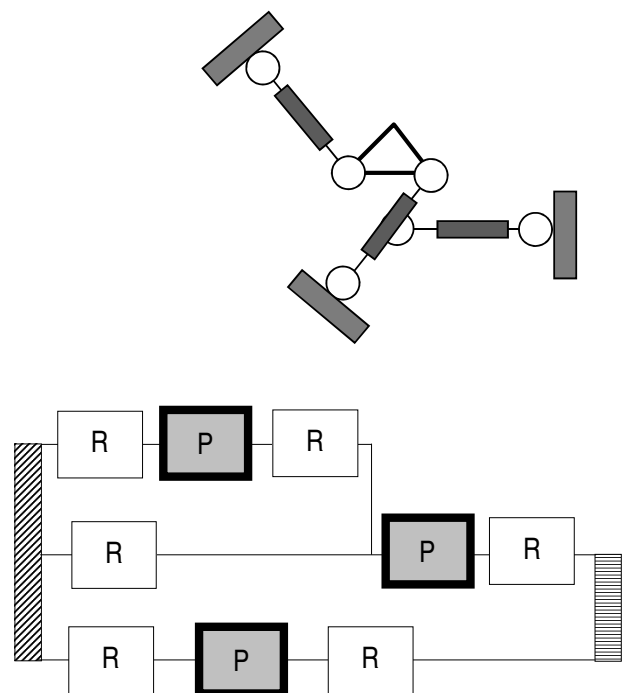
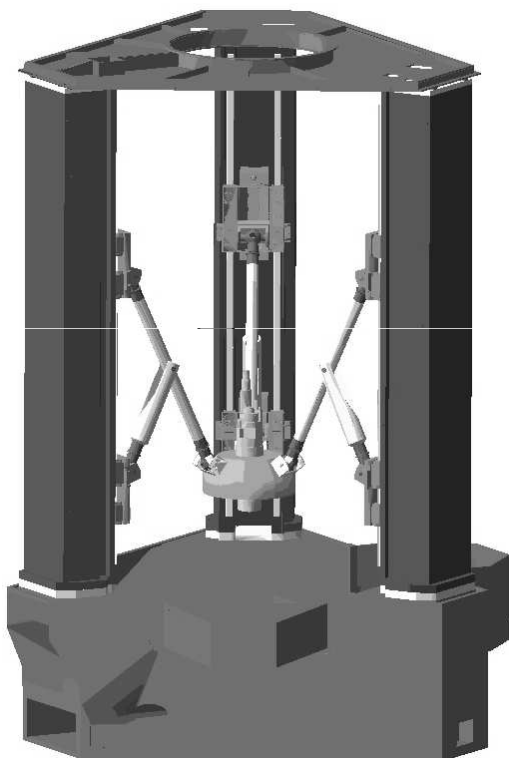
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- The PKM Landscape - With or Without a Passive Leg



- The PKM Landscape - Fully Parallel or Non-Independent Chains

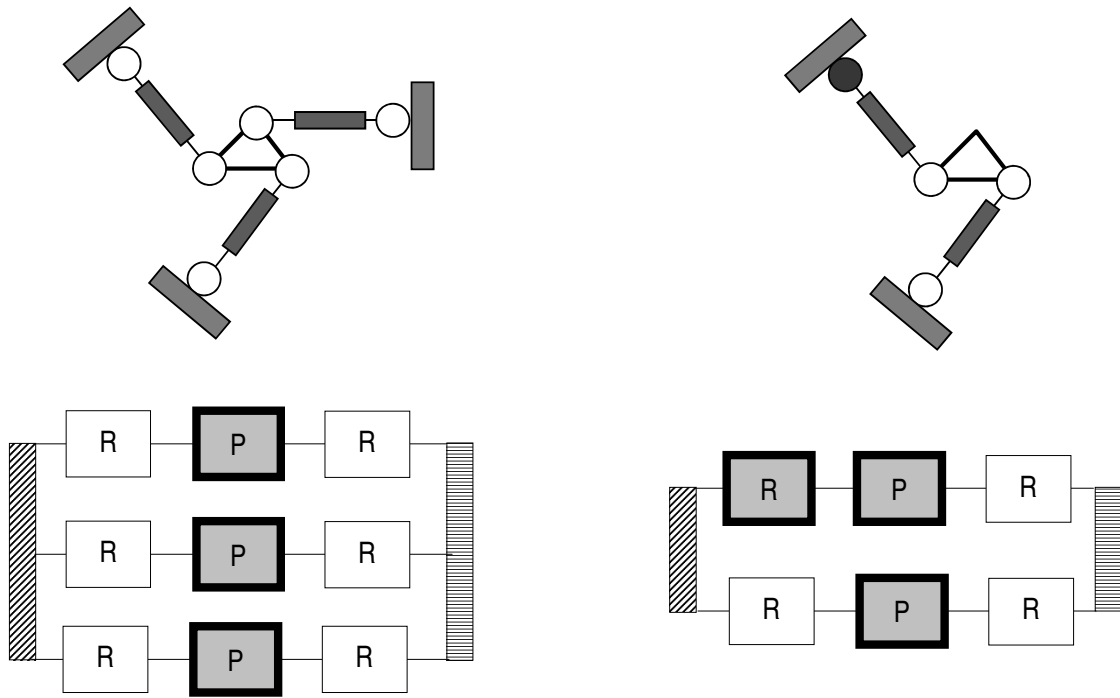




- The PKM Landscape - Fully Parallel or Non-Simple Chains

LIRMM

Guidelines for Design (65)



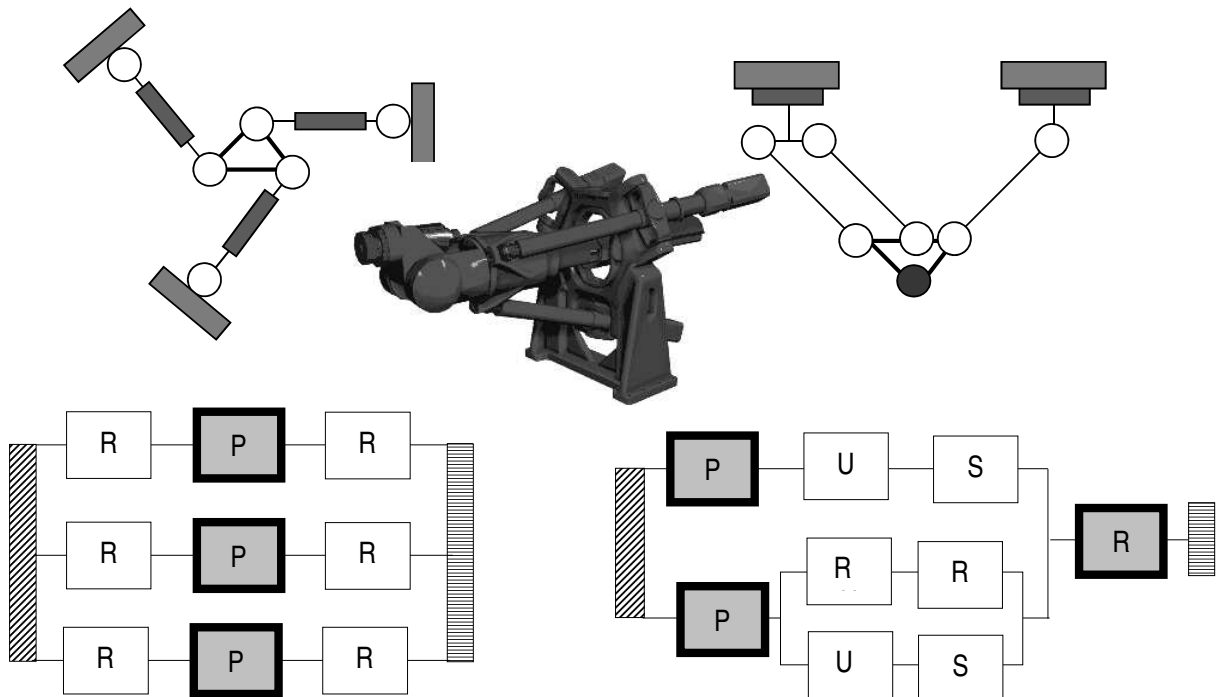
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- The PKM Landscape - Parallel or Hybrid P-S

LIRMM

Guidelines for Design (66)



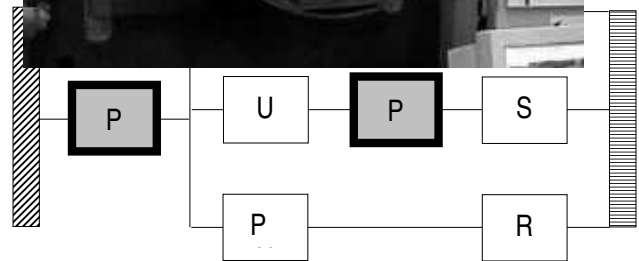
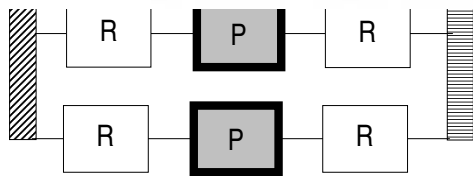
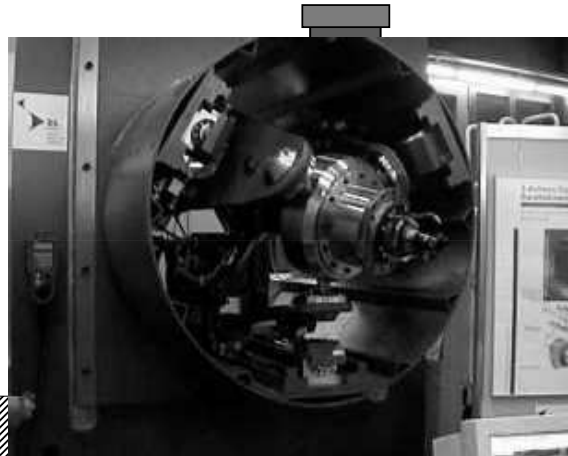
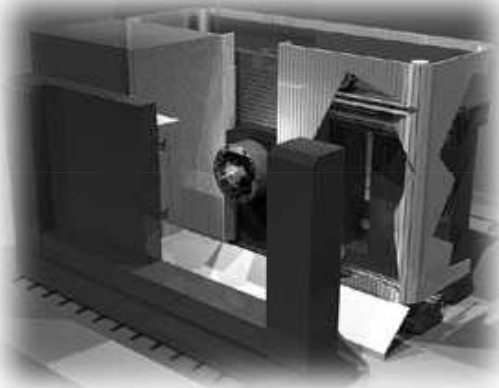
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- The PKM Landscape - Parallel or Hybrid S-P

LIRMM

Guidelines for Design (67)



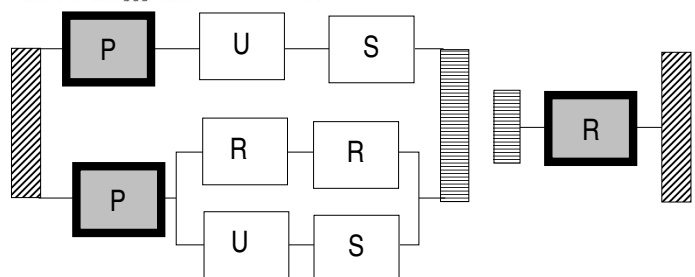
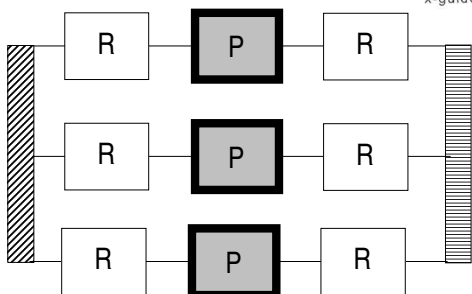
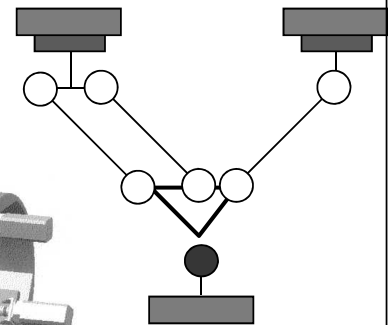
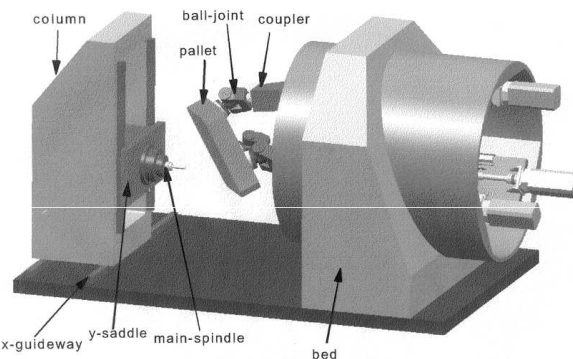
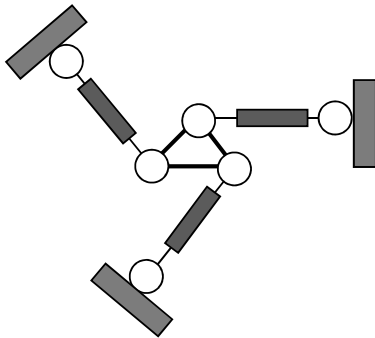
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- The PKM Landscape - Parallel or Hybrid LH-RH

LIRMM

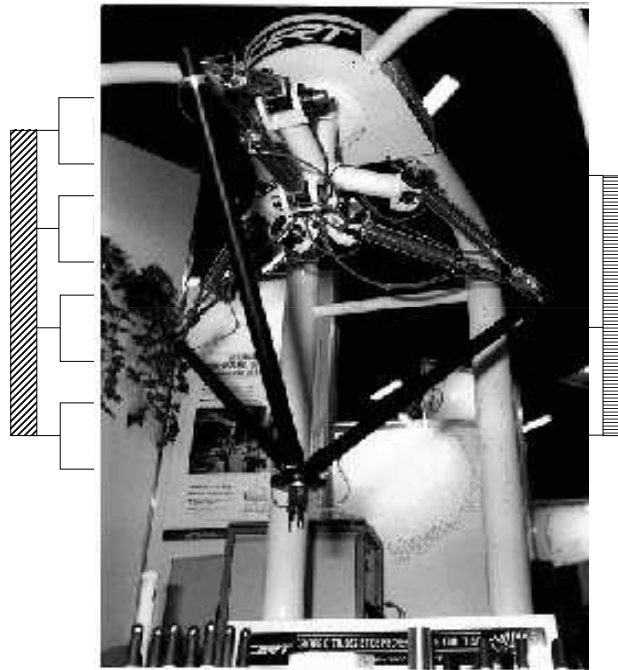
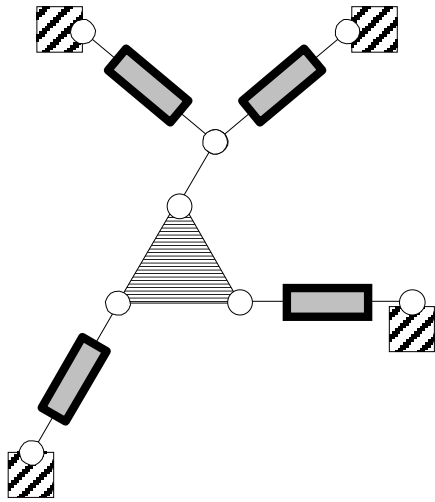
Guidelines for Design (68)



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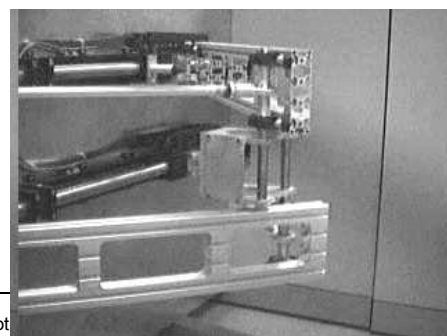
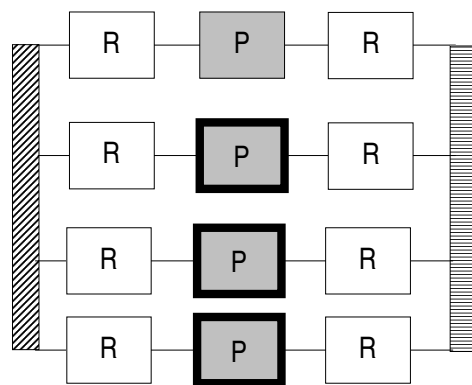
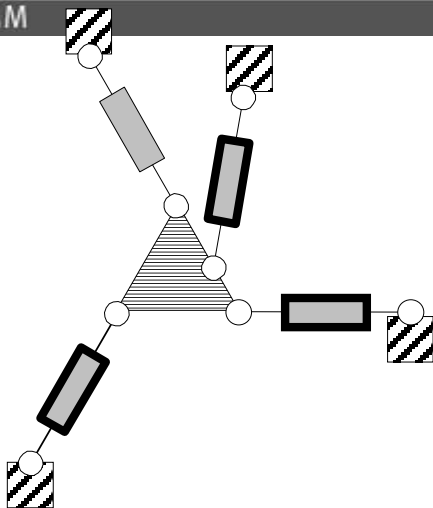
- The PKM Landscape - Kinematic Redundancy



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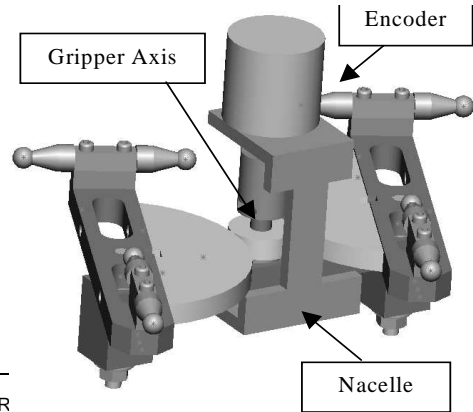
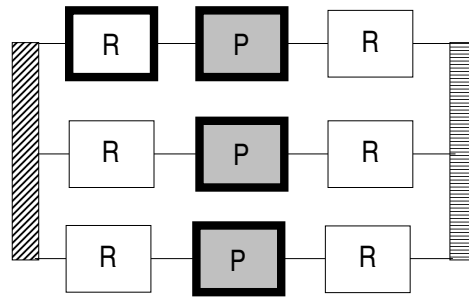
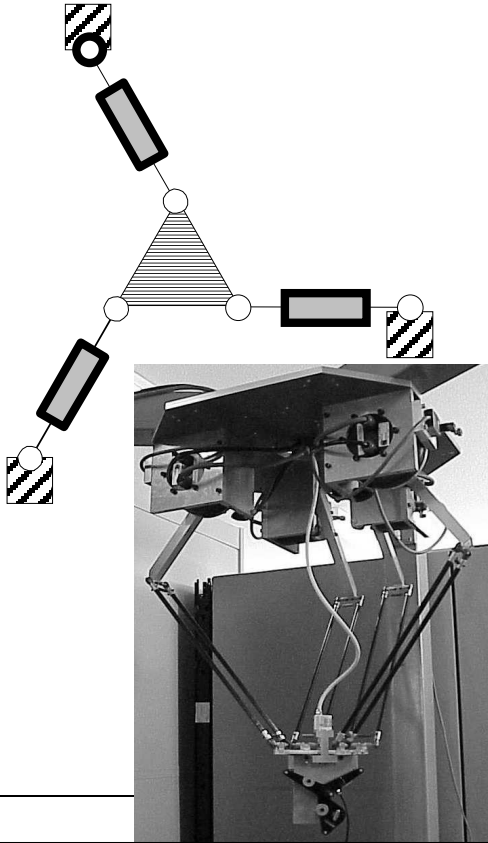
- The PKM Landscape - Actuation Redundancy



in Surgical Robot



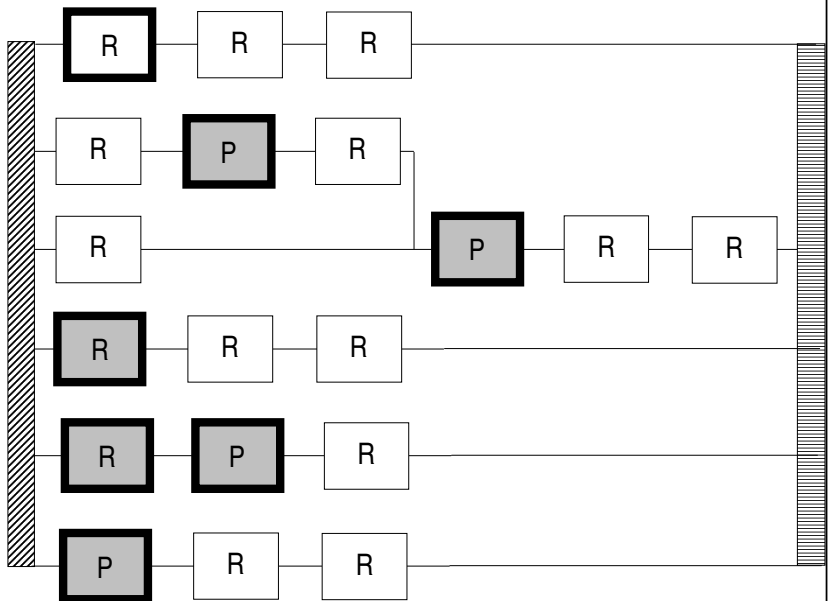
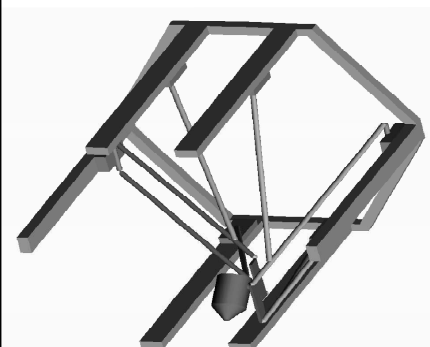
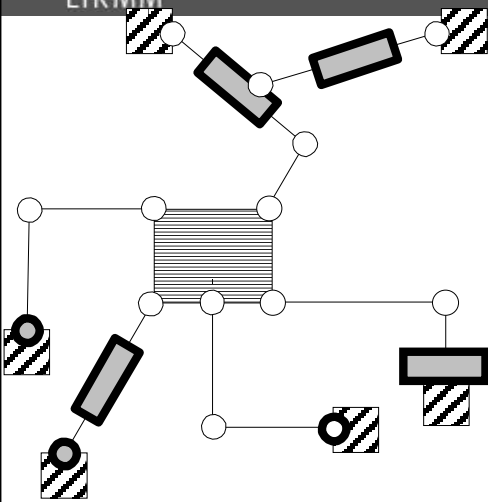
- The PKM Landscape - Measurement Redundancy



Model on Surgical R



- The PKM Landscape - No Limit!



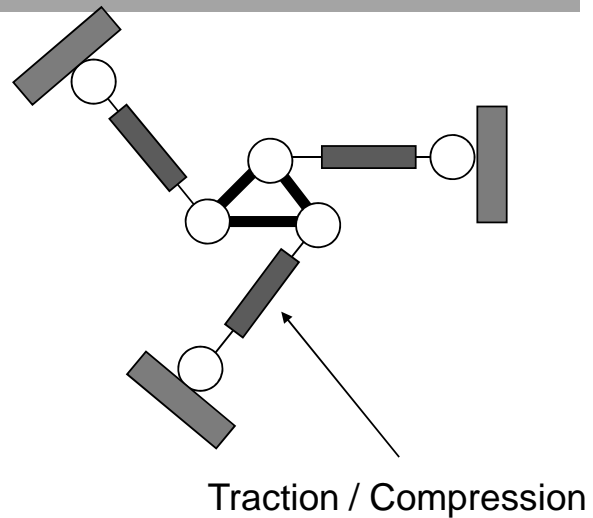
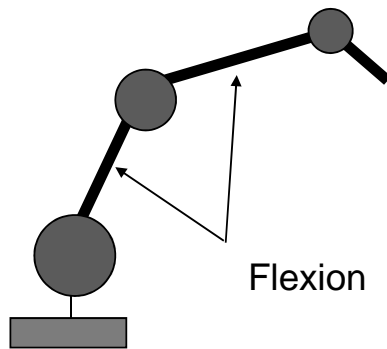


Common (Claimed) Advantages

LIRMM

Guidelines for Design (73)

- Stiffness, Accuracy, Speed, Acceleration (up to 40 g!)
- Good Weight/Load Ratio
- Lots of Common Parts
- Very good dynamic capabilities and ability to force control



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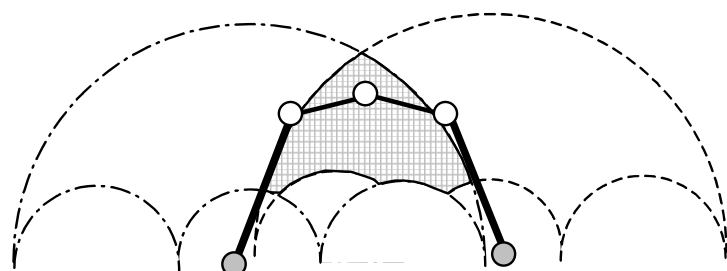
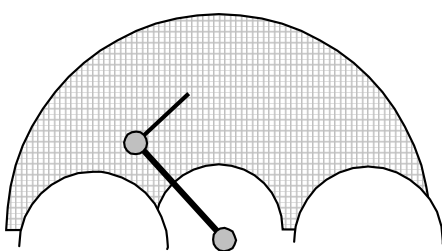


(Most) Common Drawbacks

LIRMM

Guidelines for Design (74)

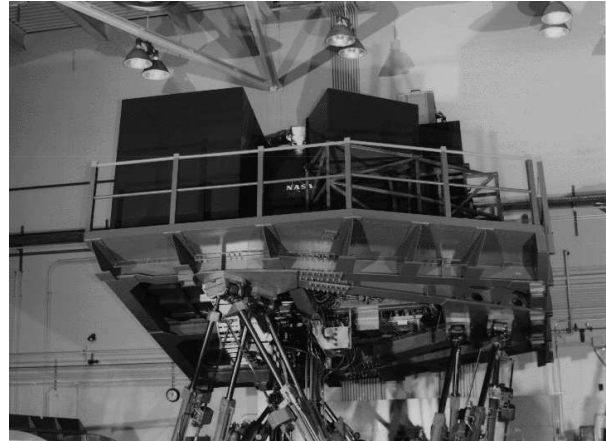
- Lots of Passive Joints
- Modeling / Singularities
- Not always supported by conventional NC
- Non classical calibration
- Too « advanced » for some markets
- Bad Foot-Print/Workspace Ratio



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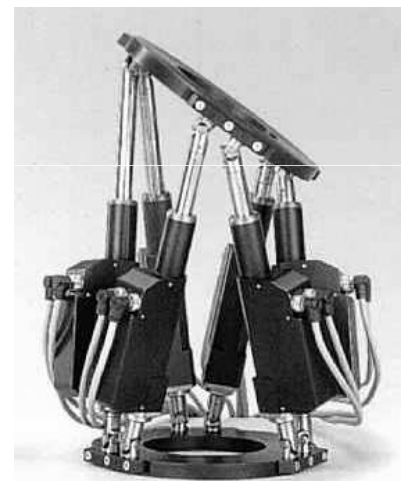
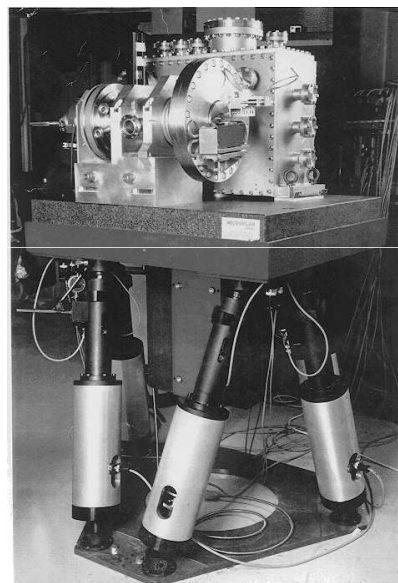
Application domains: simulators



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Application domains: positioning systems



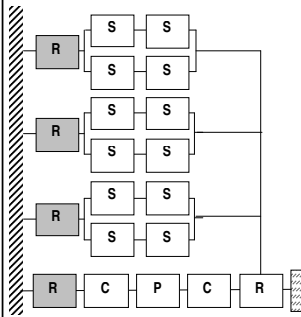
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Application domains: handling

LIRMM

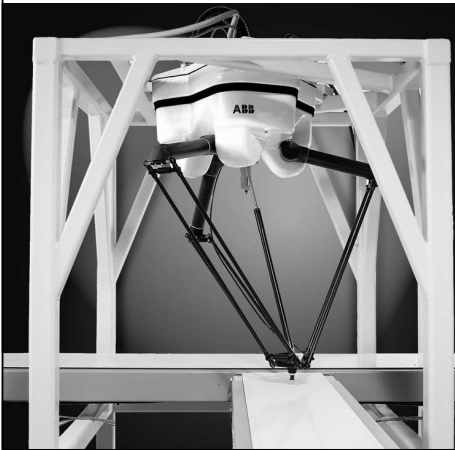
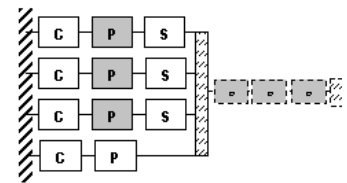
Guidelines for Design (77)



Delta



Tricept



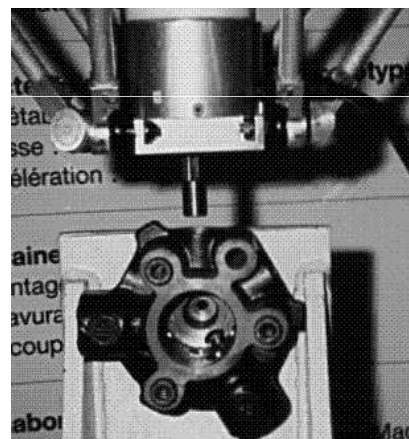
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Application domains: handling

LIRMM

Guidelines for Design (78)



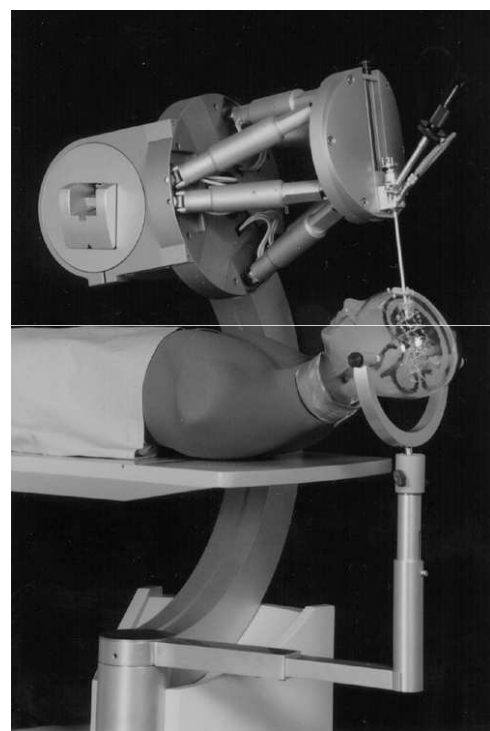
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Application domains: machine-tool

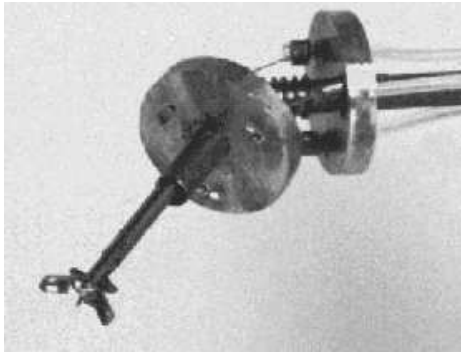


Application domains: surgery

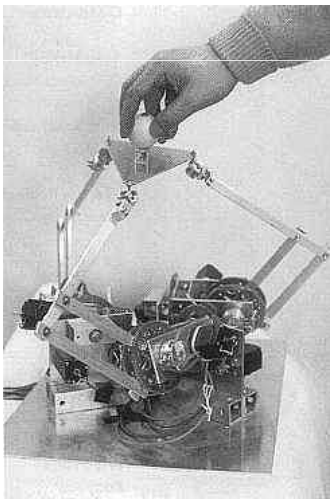




Application domains: surgery

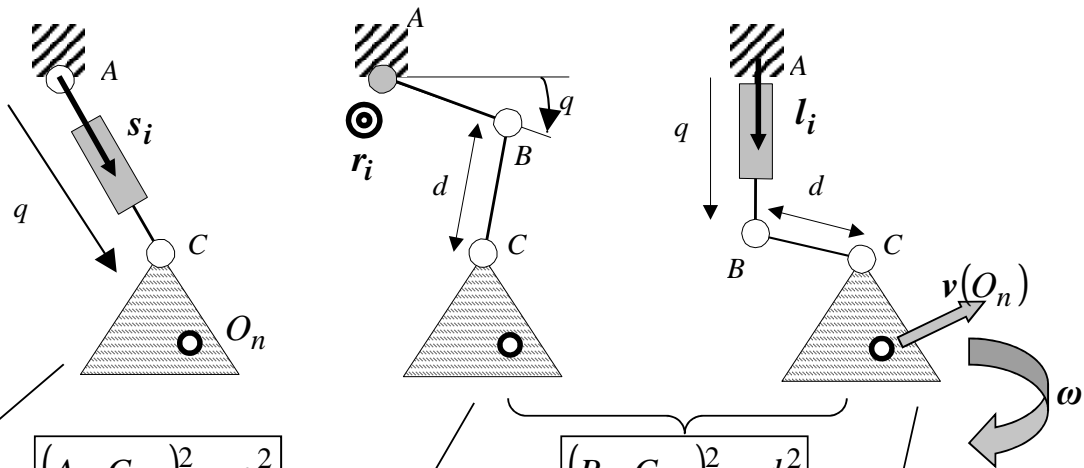


Application domains: haptic devices





IKM (from x to q)



$$(A_{i,b} C_{i,b})^2 = q_i^2$$

$$(B_{i,b} C_{i,b})^2 = d_i^2$$

$$\dot{q}_i = s_i \cdot v(O_n) + (s_i \times C_i O_n) \cdot \omega$$

$$\dot{q}_i (B_i A_i \times r_i) \cdot B_i C_i = B_i C_i \cdot v(O_n) + (B_i C_i \times C_i O_n) \cdot \omega$$

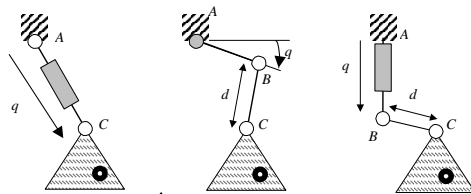
$$\dot{q}_i (l_i \cdot B_i A_i) \cdot B_i C_i = B_i C_i \cdot v(O_n) + (B_i C_i \times C_i O_n) \cdot \omega$$



Singularities (1)

$$\dot{q} = \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_k \end{bmatrix}$$

$$\dot{x} = \begin{bmatrix} v(O_n) \\ \omega \end{bmatrix}$$



$$J_q \cdot \dot{q} = J_x \cdot \dot{x}$$

$$J_x = \begin{bmatrix} b'_1 & (b_1 \times C_1 O_n) \\ b'_2 & (b_2 \times C_2 O_n) \\ \vdots & \vdots \\ b'_k & (b_k \times C_k O_n) \end{bmatrix}$$

$$J_q = Ident_k$$

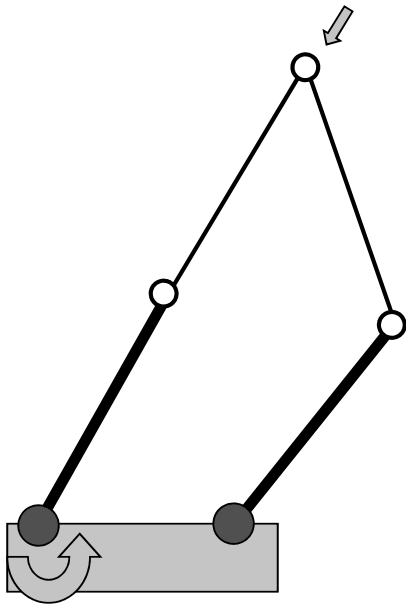
$$J_q = \begin{bmatrix} (B_1 A_1 \times r_1) \cdot b_1 & 0 & 0 & 0 \\ 0 & (B_2 A_2 \times r_2) \cdot b_2 & 0 & 0 \\ 0 & 0 & \ddots & 0 \\ 0 & 0 & 0 & (B_k A_k \times r_k) \cdot b_k \end{bmatrix}$$

$$J_q = \begin{bmatrix} l_1 \cdot b_1 & 0 & 0 & 0 \\ 0 & l_2 \cdot b_2 & 0 & 0 \\ 0 & 0 & \ddots & 0 \\ 0 & 0 & 0 & l_k \cdot b_k \end{bmatrix}$$

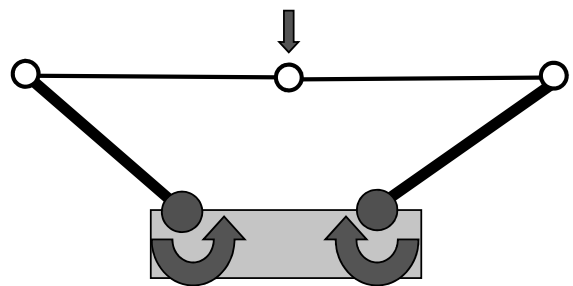


Singularities (2)

Under-mobility (serial):
motor moves → no tool motion



Over-mobility (parallel):
High motor torque → no force at tool

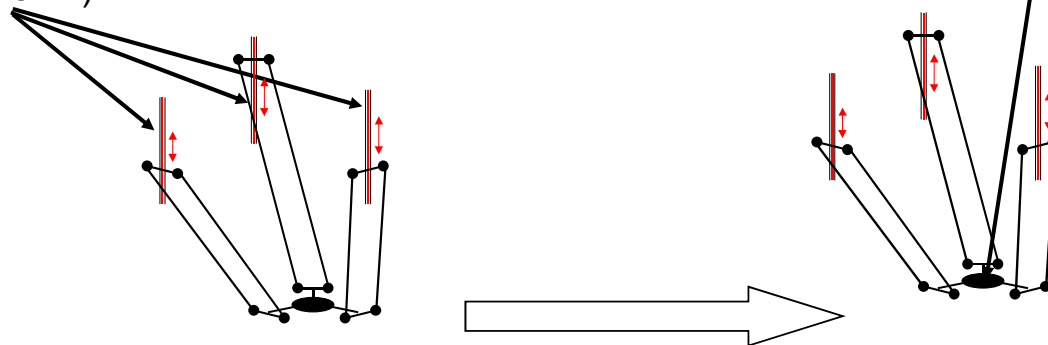


FKM (from q to x) (1)

(Drive #1,
Drive #2,
Drive #n)

IKM: closed form

(x,y,z,a,b,c)



FKM :

- Few “nice” cases with closed form
- Often: numerical resolution (polynomial of 4th, 8th, 16th, ... order)



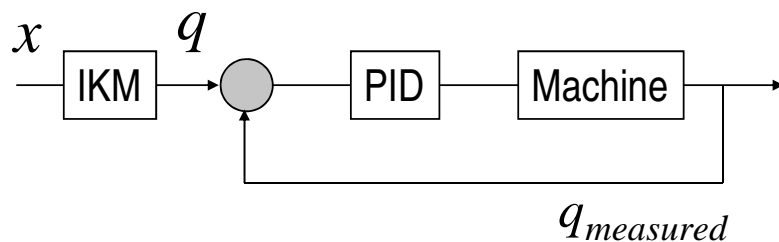
Two options for numerical solving:

- Solving the polynomial (☺ all solutions, ☹ computation cost)
- Looking for ONE solution (☺ fast, ☹ instability risk)

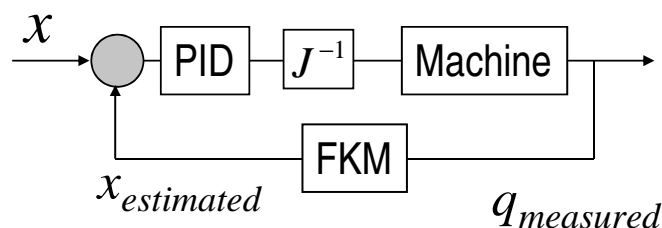
$$\begin{aligned}\hat{x}_0 &\rightarrow q_0 = \text{mgi}(\hat{x}_0) \\ \hat{x}_0 &\rightarrow (J_x, J_q)_0 \rightarrow J_0 = J_x^{-1} J_q \\ e_0 = q_{\text{mesuré}} - q_0 &\rightarrow \hat{x}_1 = \hat{x}_0 + J_0 \cdot e_0 \\ \dots \text{stop if } \|e_k\| &< \text{accuracy threshold}\end{aligned}$$

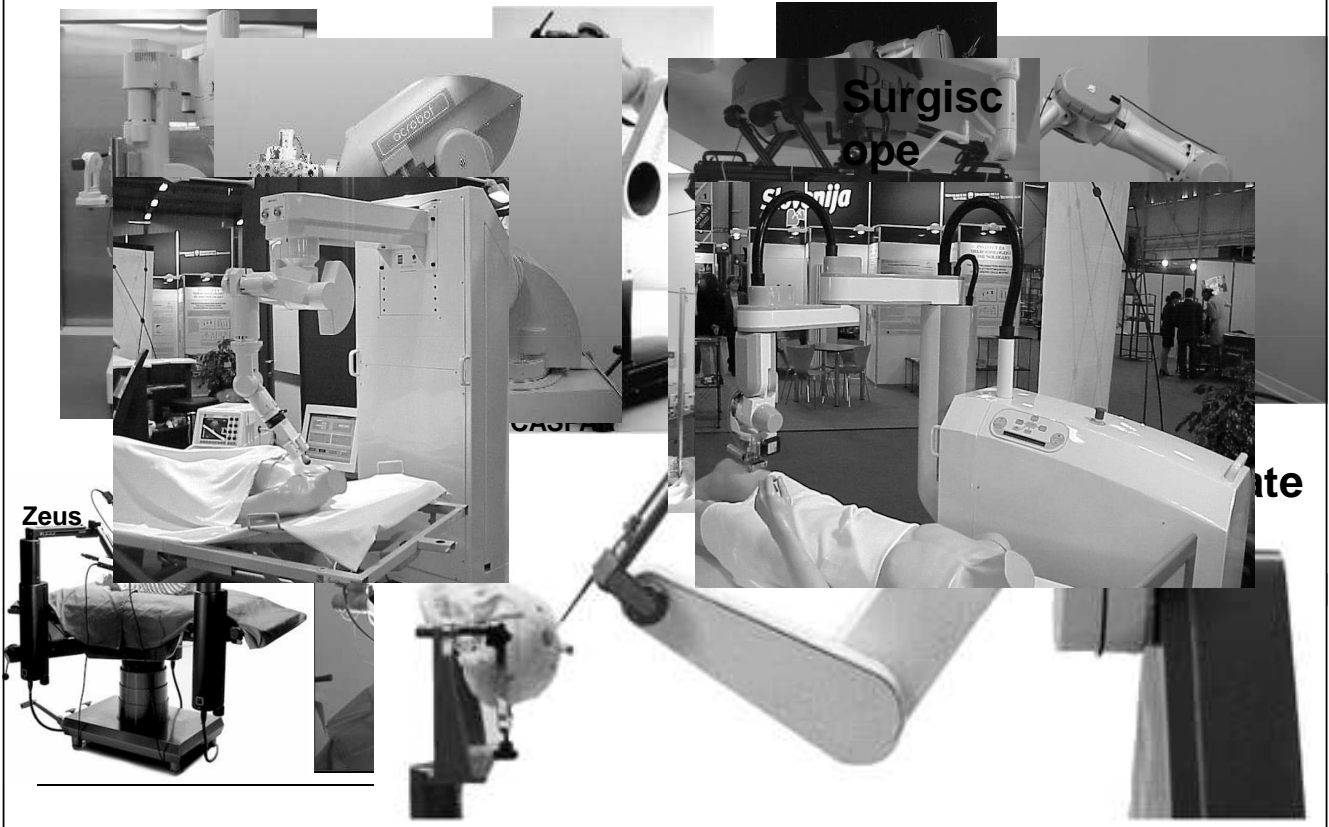


- In Joint Space with IKM



- In Cartesian Space with Jacobian





A need for multi-purpose systems

- An industry sector is mature when standards exist
 - This help to reach:
 - Lower costs
 - Better reliability
 - Portability of applications and tools
 - Creation of a “universal” knowledge



- How many dof?
- What velocity, acceleration?
 - What force?
- What kinematics?
- Above questions hold for both master and slave arms



- Nb of dof:
 - Brain → 5 dof (a point & one direction)
 - Orthopedic → 5 dof (drilling) or 6 dof (cutting)
 - M.I.S. → 5 dof extra-body + 3 dof (intra-body rotations)
 - 6 dof extra-body (if R_z is accounted for) + 2 dof (intra-body)
 - Skin grafting → 6 dof

A multi-purpose slave arm may be composed of:

- A “universal” carrier with 5 or 6 dof
- A “specific” wrist with 1 to 3 dof



Multi-purpose slave arm: speed & force

LIRMM

Guidelines for Design (93)

- Speed, acceleration
 - Brain → often works at rest
 - Skin grafting → a few mm/s
 - M.I.S. → several 100mm/s (large rotations of tool x tool length)
 - Orthopedic → a few mm/s
 - Heart → Acceleration probably $> 1g$ (if “heart-beating surgery” is considered)
- Forces:
 - Brain → ?
 - Skin grafting → 40 N ~ 80 N
 - M.I.S. → few N (+ disturbances due to the trocar)
 - Orthopedic → up to 100 N (extremely dependent on cutting param.)

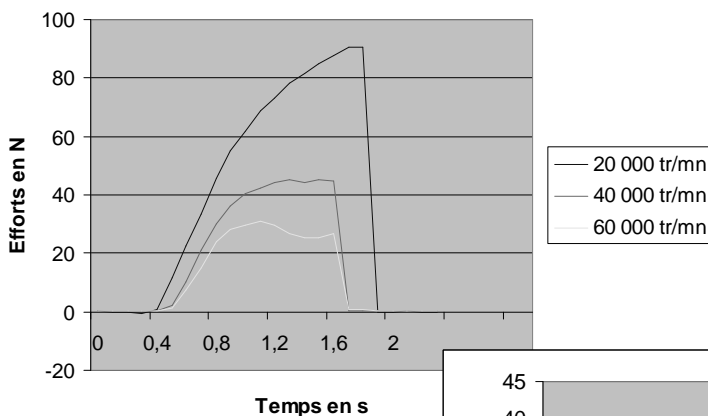
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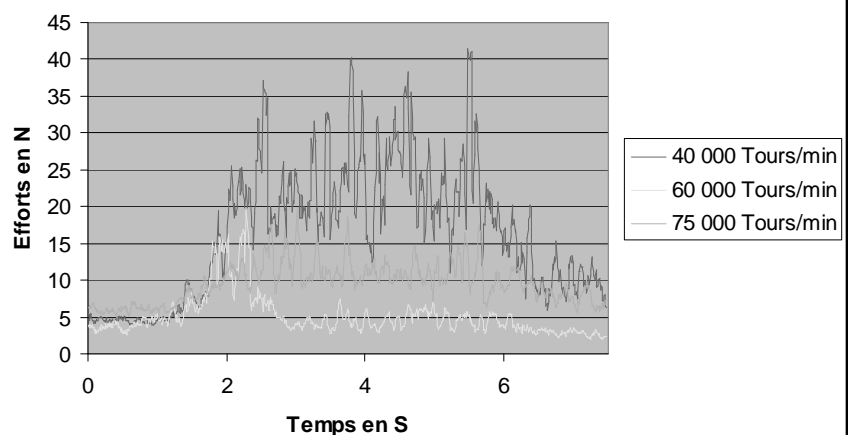
Remark: forces in machining bone

LIRMM

Guidelines for Design (94)



Milling
Tool Diameter 12.5 mm
Depth of cut 2 mm
Speed 4.0 mm/s



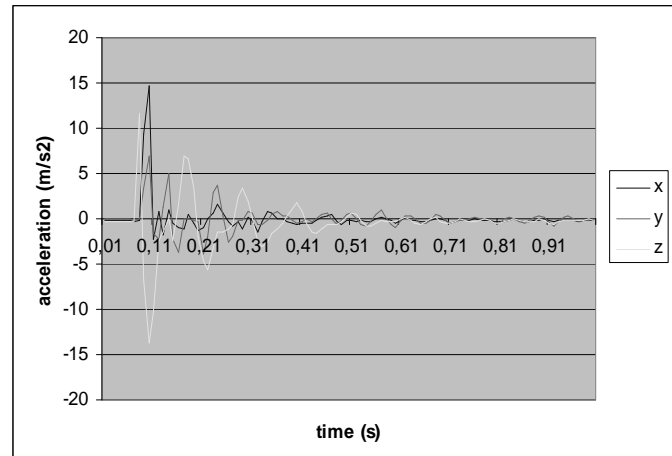
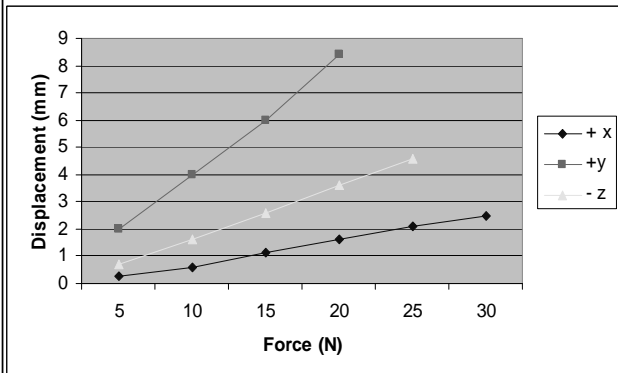
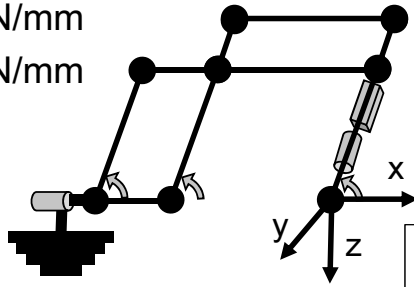


Remark: DaVinci arm is not made for bone machining

LIRMM

Guidelines for Design (95)

- $k_x = 12 \text{ N/mm}$
 - $k_y = 2,4 \text{ N/mm}$
 - $k_z = 5,4 \text{ N/mm}$
- Very low vibration frequency



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Multi-purpose slave arm: force & speed

LIRMM

Guidelines for Design (96)

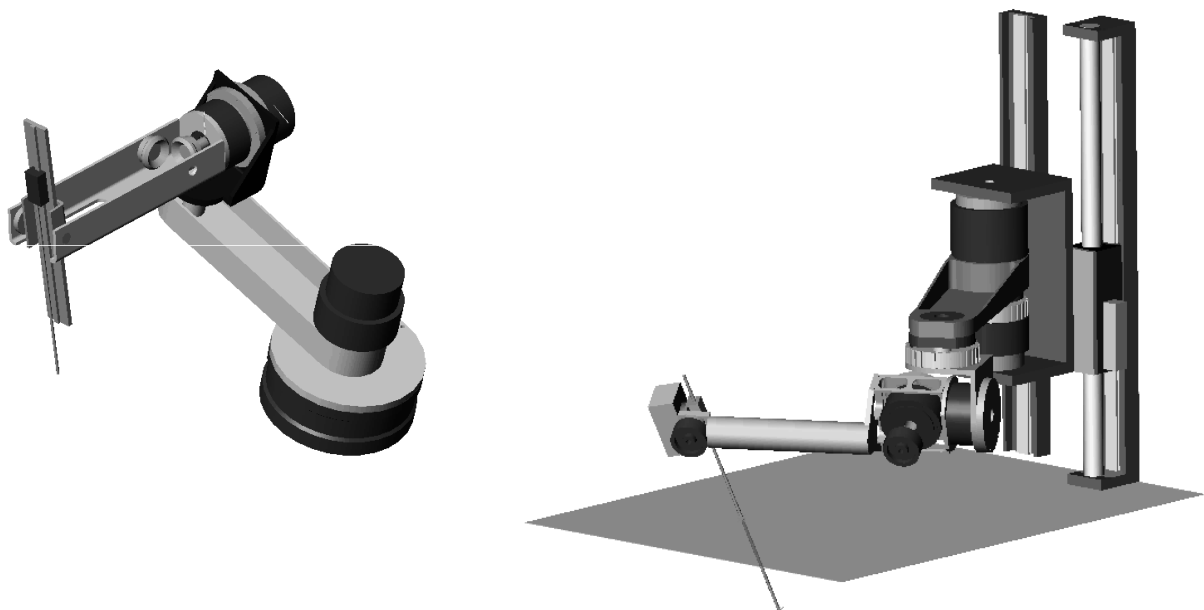
- A multi-purpose slave arm may be required to offer:
 - Good behavior at speed as low as few mm/s
 - The capability to move as fast as several 100mm/s
 - A sensitivity good enough to guarantee low forces
 - The capability to exert force up to 100N
 - Good acceleration ability (for “heart-beating surgery”)
 - Good stiffness

A multi-purpose slave arm could be based on Direct Drives
(safety issues?)

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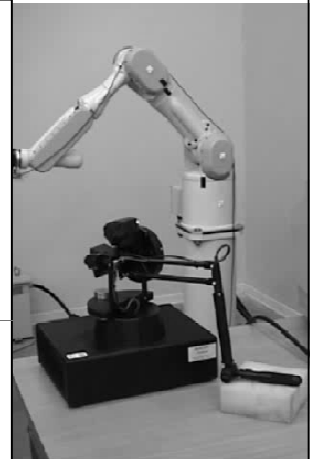
- The carrier part of a multi-purpose slave arm may be based on Scara kinematics for the following reasons:
 - Convenient fit between robot workspace and human body volume
 - Models are straightforward, even with “fancy” wrists
 - Singularities are easily managed
 - Gravity effect may not be such a big problem
 - Scara fits well with DD technology





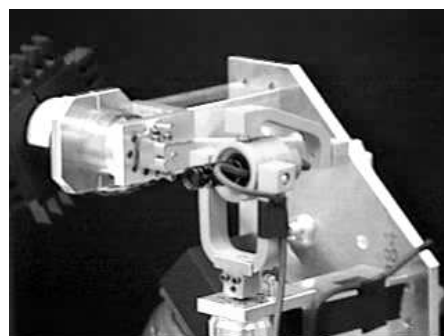
Selection of a master arm

- Dof: 6
- Range of motion
 - Translation \Leftrightarrow $[10 \text{ cm}]^3 \sim [20 \text{ cm}]^3$
 - Rotation \Leftrightarrow $> (140 \times 90 \times 120)$ degrees
- Force-feedback capable
 - Several N for rough force sensing (orthopedic)
 - $< \text{N}$ for M.I.S.
 - High dynamic, e.g. for heart surgery (“the touch of a finger on an atheromatous artery”)
- High dynamics and extreme sensitivity makes it difficult for serial arms \rightarrow incredible costs!
- No “pure” PKM exists with such a large range of motion



Selection of a master arm: the PKM way

- A multi-purpose master arm may be based on advanced PKM concepts:
 - Hybrid design
 - or
 - Redundancy
 - or
 - Both

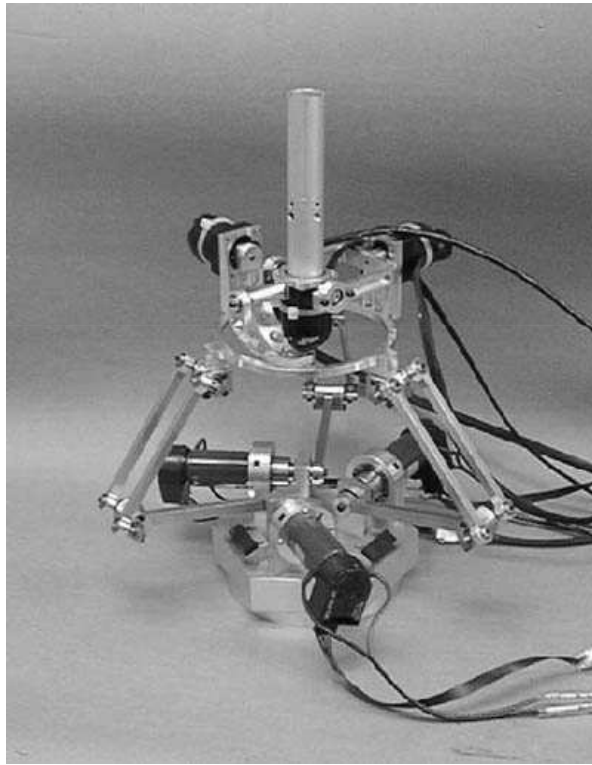




Multi-purpose master arm: potential solutions

LIRMM

Guidelines for Design (101)



Force/torque sensor
1-DOF



2-DOF five bar
spatial mechanism



3-DOF modified
DELTA mechanism

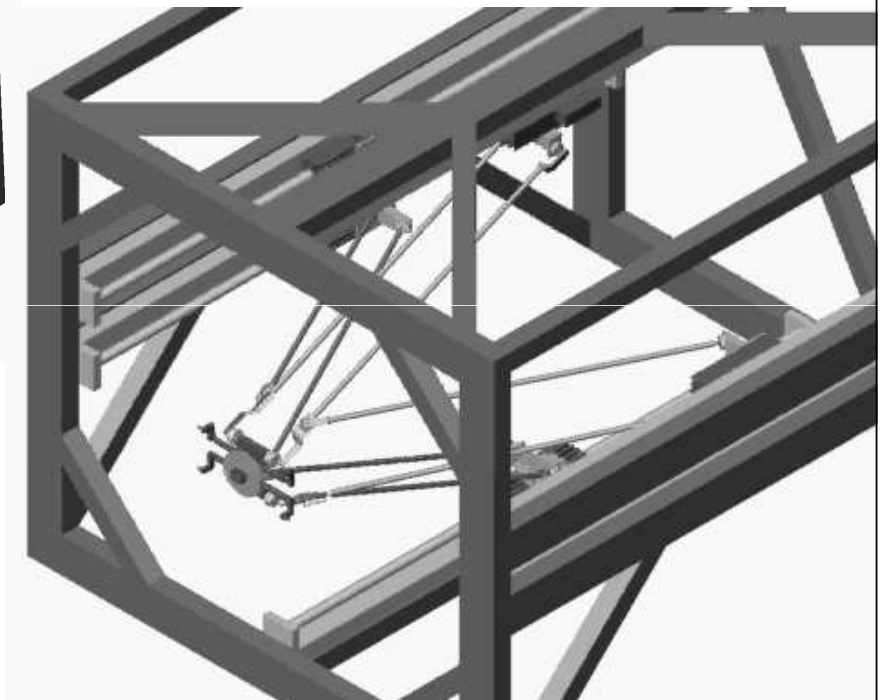
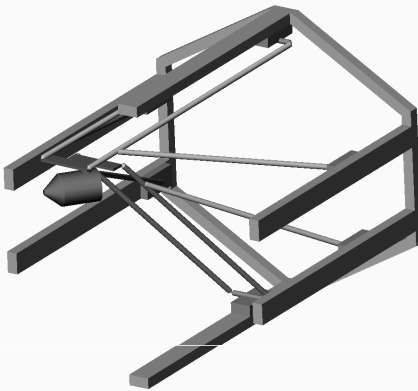
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Multi-purpose master arm: potential solutions

LIRMM

Guidelines for Design (102)



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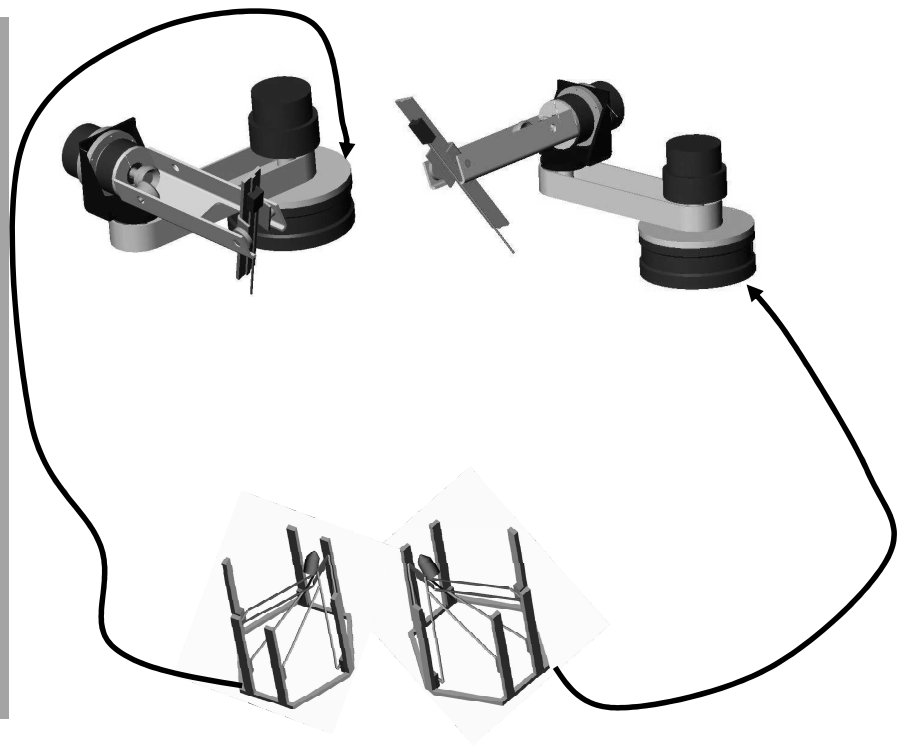


Standardized
Scara-like
DD arms
Under force control

Remotely operated by

Hybrid PKM with
Large tilting capabilities

And Carrying
Specific Wrists



Thank you !!!